Experimental Testing of Anchoring Devices for Bottom Rail in Partially Anchored Timber Frame Shear Walls With Two-Sided Sheathing

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Abstract

Källsner and Girhammar [1] have presented a new plastic design method for wood-framed shear walls at ultimate limit state. This method allows the designer to calculate the load-carrying capacity of shear walls partially anchored, where the leading stud is not fully anchored against uplift.

The anchorage system of shear walls is provided from anchor bolts and hold downs. Anchor bolts provide horizontal shear continuity between the bottom rail and the foundation. Hold downs are directly connected from the vertical end stud to the foundation. When hold downs are not provided, the bottom row of nails transmits the vertical forces in the sheathing to the bottom rail (instead of the vertical stud) where the anchor bolts will further transmit the forces into the foundation.

Because of the eccentric load transfer, due to forces acting in the same vertical plane, transverse bending is created in the bottom rail and splitting often occurs.

It is important to evaluate this cross-wise bending and to ensure that no brittle failure occur in the bottom rail.

The bottom rail is experimentally studied with respect to two primary failure modes, splitting along the bottom of the bottom rail due to cross-wise bending and splitting along the edge side of the bottom rail due forces perpendicular to the grain from the sheathing-to-framing connections.

The parameters varied are the size of the washer and the orientation of the pith.

The bottom rail was subjected to loading perpendicular to grain through two-sided sheathing.

In this report the different set of series are presented. Five sets were conducted depending on the size of the washer and in each set the pith was placed upwards and downwards.

The tests showed three different failure modes. In addition to the failure modes that the testing program was aimed at, splitting along the bottom or side of the bottom rail, the final failure was also due to plastic bending and withdrawal of the sheathing-to-framing nails.

The results show that the size of the washer has a significant influence on the maximum load and the failure modes. The results show also that the orientation of the pith have a significant influence on the maximum load.

Key words: timber shear walls, partially anchored, sheathing-to-framing joint, bottom rail, cross-wise bending, splitting of bottom surface, splitting of side surface.

Acknowledgements

The experiments of this report were carried out at Umeå University, Sweden, in June 2011.

Bo Källsner and Ulf Arne Girhammar have initiated this study as part of their research work on a plastic design method for partially anchored light-frame shear walls. Per-Anders Daerga has planned the test series. Giuseppe Caprolu has performed the experiment and written the report.

I would like to thanks Bo Källsner and Ulf Arne Girhammar for reviewed the report and Helena Johnsson for reading and commenting the manuscript.

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Introduction

Background

Källsner and Girhammar [1] have presented a new plastic design method for wood-framed shear walls at ultimate limit state. This method allows the designer to calculate the load-carrying capacity of shear walls partially anchored, where the leading stud is not fully anchored against uplift.

The anchorage system of shear walls is provided from anchor bolts and hold downs. Anchor bolts provide horizontal shear continuity between the bottom rail and the foundation. Hold downs are directly connected from the vertical end stud to the foundation. When hold downs are not provided, the bottom row of nails transmits the vertical forces in the sheathing to the bottom rail (instead of the vertical stud) where the anchor bolts will further transmit the forces into the foundation.

Because of the eccentric load transfer, due to forces acting in the same vertical plane, transverse bending is created in the bottom rail and splitting often occurs.

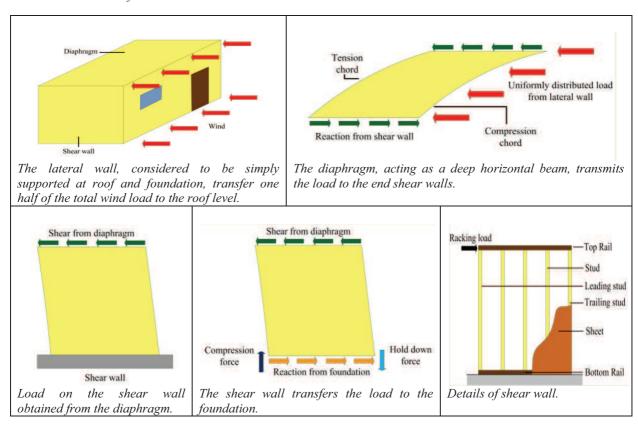
Characteristics of shear walls

A shear wall is an in-plane structural element designed to transmit forces in its own plane. Horizontal roof and floor diaphragms are designed to distribute lateral loads to the shear wall elements, which in turn carry the loads to the foundations. The shear walls are subjected to shear forces at roof level from the roof diaphragm, and resisted by shear and normal reactions at the foundations. Shear walls must be anchored to the foundation to resist uplift forces.

A shear wall in timber construction is a load-bearing wall that is designed to carry racking loads in the plane of the wall (shear loads) in addition to the vertical loads.

The horizontal forces create an overturning moment on the shear wall and therefore create uplift forces on one side and compression on the other side of the wall. The strength of the wall is dependent upon three components: timber frame members, sheathing and fasteners.

Table 1: Behaviour of shear wall



Details of the bottom rail

The main difference between fully and partially anchored shear walls is the presence in the second case of uplift of the studs of the wall, especially of the leading stud.

In fully anchored shear walls the uplift is prevented by some kind of tying down device at the leading stud. This will result in a concentrate force at the end of the wall. In partially anchored shear walls there are no device between the leading stud and foundation. The uplift is resisted by the sheathing-to-framing joints along the bottom rail. This will result in a distributed force on the bottom rail and there is some uplift of the studs of the wall (*see Figure 1*).

In the latter case the bottom rail will be subject to uplift forces that cause a tension stresses perpendicular to the grain and crosswise bending (see Figure 1).

Due these stresses brittle failure of the bottom rail may occur. In order to have the correct distribution of the forces for partially anchored shear walls, brittle failure of the bottom rail should be avoided.

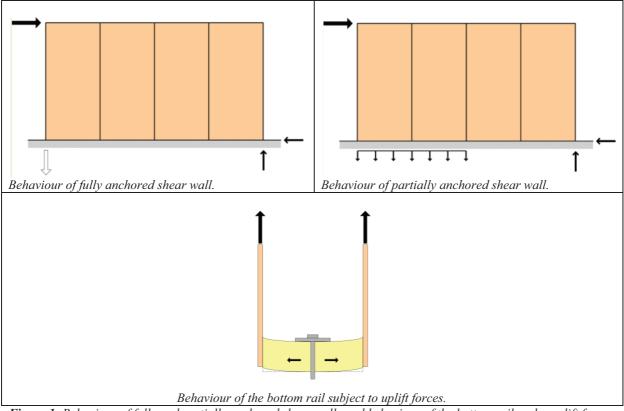


Figure 1: Behaviour of fully and partially anchored shear walls and behaviour of the bottom rail under uplift forces

Aim and scope

The overall study focuses on the study of a new plastic design method [1] of wood-frame shear walls at ultimate limit state. This method allows to calculate the load-carrying capacity of shear wall partially anchored, where the leading stud is not anchored against the uplift.

The aim of this study is to design the bottom rail against forces from sheathing-to-framing joint. The bottom rail should be designed in the ultimate limit state. Both shear force and cross-wise bending, due the absence of hold down, are present in the bottom rail. It is also important to determine the conditions for the bottom rail for the plastic method to work.

This study focuses on double-sided sheathing. Earlier one-sided sheathing was studied [2].

In order to use the plastic method it is necessary to ensure two main conditions: avoid brittle failure of the bottom rail and to ensure a ductile behaviour of the sheathing-to-framing joint.

The scope of this report is to present results of laboratory tests of the bottom rail subjected to uplift forces through sheathing-to-framing joints. Two primary failure modes are in focus, splitting along the bottom of the bottom rail due to cross-wise bending and splitting along the edge side of the bottom rail due forces perpendicular to the grain from the sheathing-to-framing connections.

The bottom rail was subjected to loading perpendicular to grain through two-sided sheathing.

The experimental work was conducted at Umeå University during June 2011.

Test setup and material

Test specimen

The specimens were built with a rail of length 900 mm and with a cross section of 45×120 mm, joined with hardboard sheet of $500 \times 900 \times 8$ mm.

At first it was thought of planing the top and bottom surface of the rail, in order to eliminate any influence of cupping and possible pre-cracking, when tightening the anchor bolts, on the ultimate load. However it was not necessary because the surfaces of the bottom rail were acceptable with regard to flatness.

The rails were kept enclosed in a plastic cover in lab from 29 March 2011 to September 2011. The temperature in lab was about 20° C. They were already cut from the factory, therefore it was impossible to choose rails cut from the same board in order to have rails with the same density.

The specimens were assembled manually. They were usually assembled the evening before the day of testing. Sometime this was not possible (see Appendix B for a chronological summary of the conduction of the tests).

Test program

A total of 64 specimens were planned to test but due to a mistake during the testing of Set 1 (*tested with the inclined bars in the lifting device*) it was necessary to repeat that Set and Set 1-BIS was added to the test program and a total of 80 specimens have been tested. The results of Set 1 are still presented in this report.

The table below shows the test program:

Table 2: Test program

| Series | Anchor bolt position | Set | Size of washer [mm] | Number of tests | Distance from washer edge to rail edge [mm] |
|--------|----------------------|-------|---------------------------|------------------|--|
| | | 1 | 40x40x15 | 16 ¹⁾ | 40 |
| | Centre | 1-BIS | 40x40x15 | $16^{1)}$ | 40 |
| 4 | 60 mm from | 2 | 60x60x15 | $16^{1)}$ | 30 |
| | sheathing | 3 | 80x70x15 | 16 ¹⁾ | 20 |
| | | 4 | 100x70x15 | 16 ¹⁾ | 10 |

⁸ specimens with the pith downwards and 8 upwards

Material properties

The following materials were used for the specimens:

- Bottom rail: Spruce (Picea Abis), C24, 45x120 mm;
- Sheathing: Hardboard, C40, 8 mm (wet process fibre board, HB.HLA2, Masonite AB);
- Sheathing-to-timber joints: Annular ringed shank nails, 50x2.1 mm (Duofast, Nordisk Kartro AB). The joints were nailed manually and the holes were pre-drilled, 1.7 mm. Nail spacing was 25 mm or 50 mm. Edge distance was 22.5 mm along the bottom rail;
- Anchor bolt: Ø12 (M12). The holes in the bottom rail were pre-drilled, 13 mm.

Moisture content and density

After each test, material samples were taken from the test specimens (only for the rail). The moisture content and density of the bottom rail were determined according to recommendations of ISO 3130:1975 and ISO 3131:1975 respectively.

The moisture content (ω) was calculated according to the following formula (ISO 3130):

$$\omega = \frac{m_1 - m_0}{m_0} \cdot 100 \, [\%]$$

where:

- m_1 is the mass of the test piece before the drying [g];
- m_0 is the mass of the test piece after the drying [g].

The density of the bottom rail (ρ) was calculated according to the following formula (ISO 3031):

$$\rho = \frac{m_0}{V_W} \left[\frac{kg}{m^3} \right]$$

where:

- m_0 is the mass of the test piece after the drying [g];
- $-V_{\rm w}$ is the volume of the test piece before the drying [m³, cm³].

The moisture content and density were measured the same day of the test. Sometime due different problems this was not possible and they were measured some days later (*see appendix for a chronological summary of the conduction of the tests*).

Test setup

The bottom rail was fixed to a steel plate simulating the foundation which in turn was welded to a steel structure. The connection between bottom rail and steel plate was made through two anchor bolts. To tighten the bolt a torque moment of 50 Nm was used. A square or rectangular washer of high rigidity was inserted between the bottom rail and the head bolt. Its size and shape varied for the set tested.

A tensile load with a rate of 2 mm/min was applied by a hydraulic piston (static load capacity 100 kN) through two load distribution C steel beams attached to the upper panels by four bolts Ø 16 for each panel (see Figures 2 and 3 for test setup).



Figure 2: Test setup



Figure 3: Test setup, connection panels – lifting device by bolts

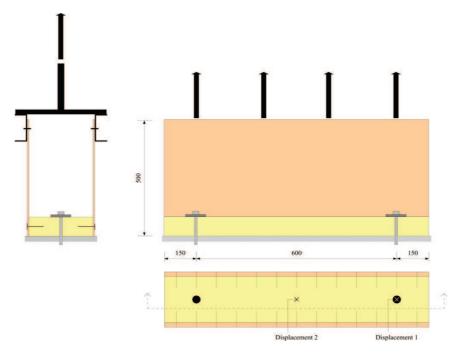


Figure 4: Specimen and test setup

Two displacements were measured using a Linear Voltage Displacement Transducer (LVDT) during the tests. These displacements are called *Displacement 1*, which measured the movement of the washer that was positioned on the upper surface of the washer on the side 1, and *Displacement 2*, which measured as the upward movement of the upper surface of the rail in the line of the anchor bolts in the middle of the distance between the anchor bolts (see Figures 4, 5 and 6).

However the displacement 1 was too small to measure and this has given some problem during recording of data. Plotting the graph load vs. displacement during the post process the line plotted appears disturbed and it is impossible to understand the real curve trend.

The rails are free to rotate during loading, i.e. the inclined bars are removed from the lifting device (see Figure 7 and 8). This provides a well-defined boundary condition. However by mistake Set 1 was tested before cutting the inclined bars and it was retested in Set 1-BIS (see Figure 9 and 10). The results of Set 1 are also presented in this report and compared with Set 1-BIS, in order to evaluate the influence of different boundary conditions.



Figure 5: position of the two LVDT on the upper surface of the bottom rail



Figure 6: position of LVDT recording displacement 1

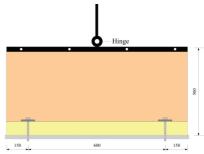


Figure 7: lifting device free to rotate during loading



Figure 8: lifting device free to rotate during loading

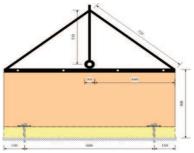


Figure 9: lifting device with inclined bars used for Set 1



Figure 10: lifting device with inclined bars used for Set 1

Test results

The load vs. time and load vs. displacement graphs are displayed for each test in Appendix A. Moreover other data and test results, as well as figures for each test, are displayed. Type of failure;

- Failure load;
- Displacement 1 and 2 at failure (displacement 1 measured the movement of washer surface on the side 1 in line of the anchor bolt. Displacement 2 measured the upward movement of the upper surface of the rail in the line of the anchor bolts in the middle of the distance between the anchor bolts);
- Distance from crack to edge, side 1 and 2 (see Figure 11);
- Distance from crack to anchor bolt, side 1 and 2 (see Figure 11);
- Moisture;
- Density.

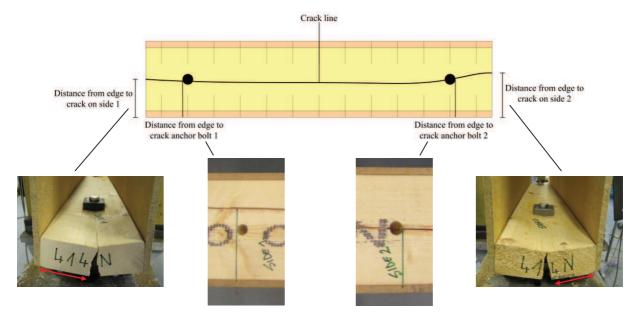


Figure 11: Example of distance between the edge of the bottom rail and crack line on side 1 and 2, and example of distance between the edge of the bottom rail and crack line at anchor bolt position on side 1 and 2

In order to identify the specimen the Swedish convention is used where N means ner (downwards in English) and U means Upp (upwards in English) according to pith orientation.

Failure modes

Different failure modes were found during the tests. They were dependant on the washer size. In total three primary failure modes were observed.

Failure mode 1: failure due to splitting of the underneath side of the bottom rail (see Figure 12);

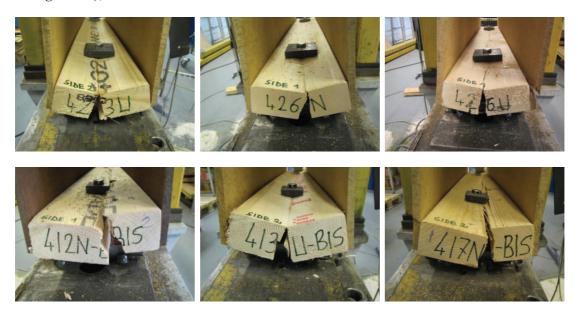


Figure 12: Some example of failure mode 1, splitting of the underneath side of the bottom rail

- <u>Failure mode 2:</u> failure due to splitting along the edge side of the bottom rail (see Figure 13);

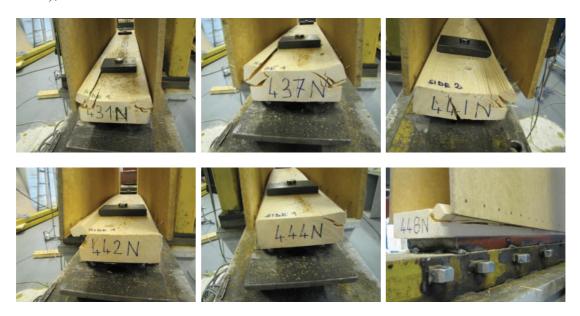


Figure 13: Failure mode 2, splitting along the edge side of the bottom rail

- Failure mode 3: failure due to pull-out of nails (see Figure 14);



Figure 14: Failure mode 3, pull-out of nails

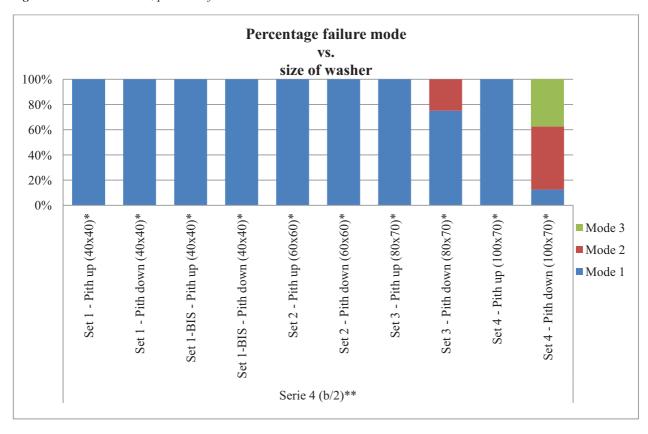


Figure 15: *Size of washer [mm], **Bolt position (where b is the width of the bottom rail, 120 mm). Failure mode 1: splitting of the bottom rail; failure mode 2: splitting of the bottom rail along the line of the nails between the anchor bolts; failure mode 3: pull-out of nails

Load vs. time and load vs. displacement curves

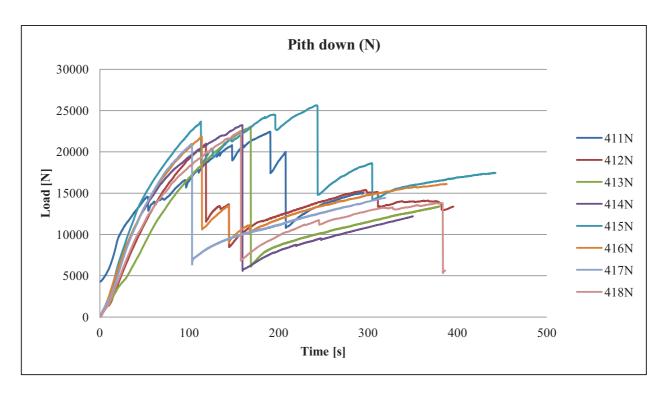


Figure 16: Load vs. time curves for bottom rail with pith down of Series 4 – Set 1. 8 failure mode of type 1

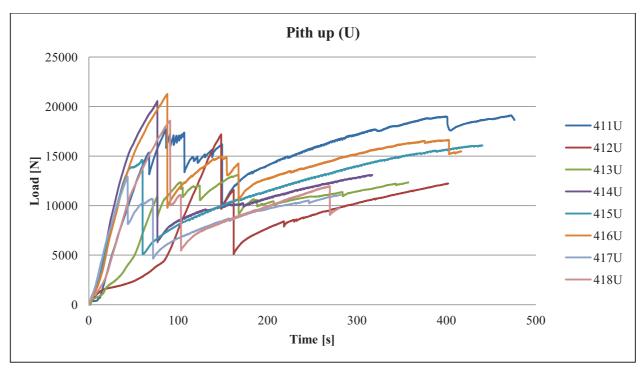


Figure 17: Load vs. time curves for bottom rail with pith up of Series 4 – Set 1. 8 failure mode of type 1

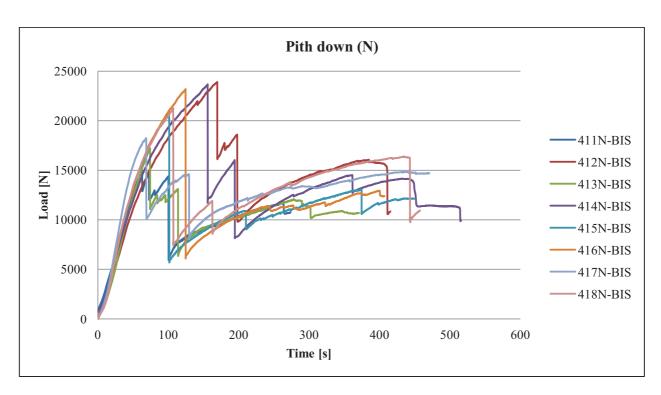


Figure 18: Load vs. time curves of bottom rail with pith down of Series 4 – Set 1-BIS. 8 failure mode of type 1

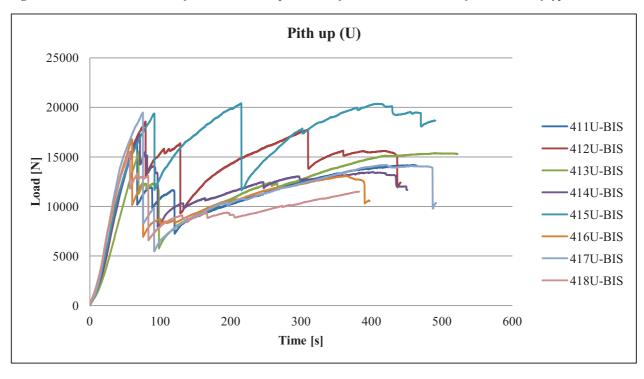


Figure 19: Load vs. time curves of bottom rail with pith up of Series 4 – Set 1-BIS. 8 Failure mode of type 1

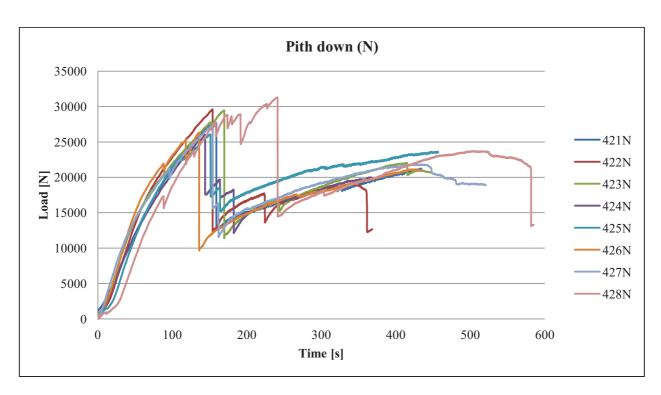


Figure 20: Load vs. time curves of bottom rail with pith down of Series 4 – Set 2. 8 failure mode of type1

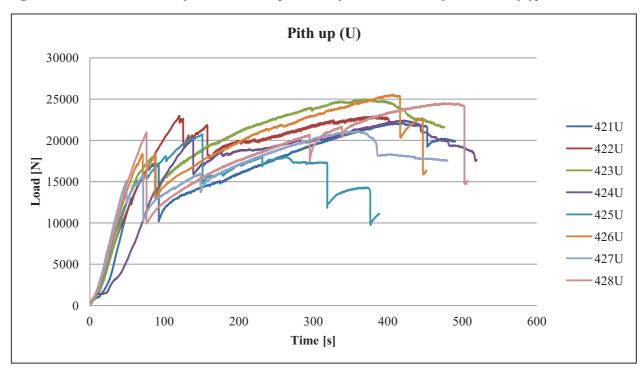


Figure 21: Load vs. time curves of bottom rail with pith up of Series 4 – Set 2. 8 failure mode of type 1

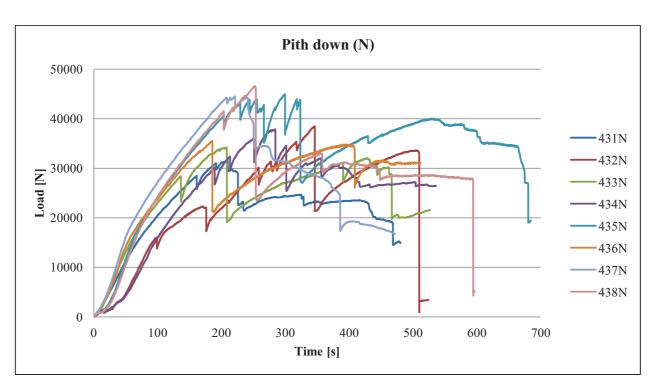


Figure 22: Load vs. time curves of bottom rail with pith down of Series 4 – Set 3. 6 failure mode of type 1 and 2 of type 2

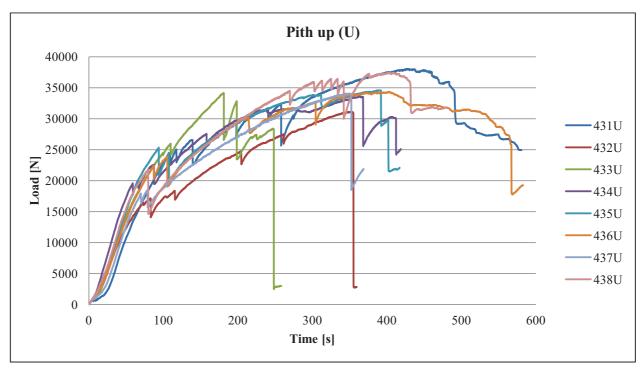


Figure 23: Load vs. time curves of bottom rail with pith up of Series 4 – Set 3. 8 failure mode of type 1

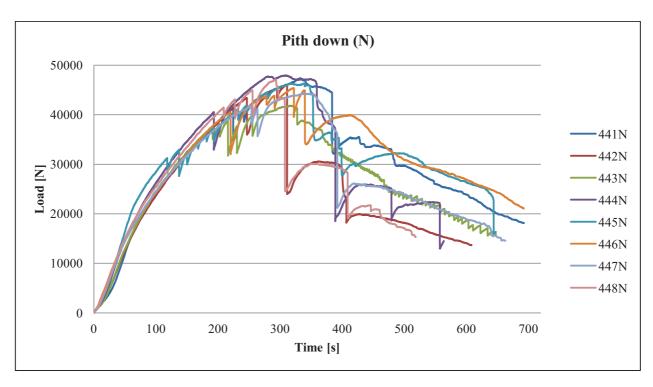


Figure 24: Load vs. time curves of bottom rail with pith down of Series 4 – Set 4. 1 failure mode of type 1, 4 failure mode of type 2 and 3 failure mode of type 3

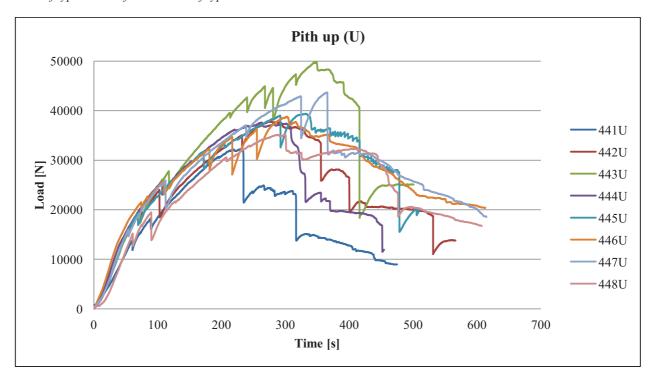


Figure 25: Load vs. time curves of bottom rail with pith up of Series $4 - Set \ 4$. 8 failure mode of type 1 (see Appendix B notes $^{(1),(2)}$ and $^{(3)}$ about the type of failure of this set)

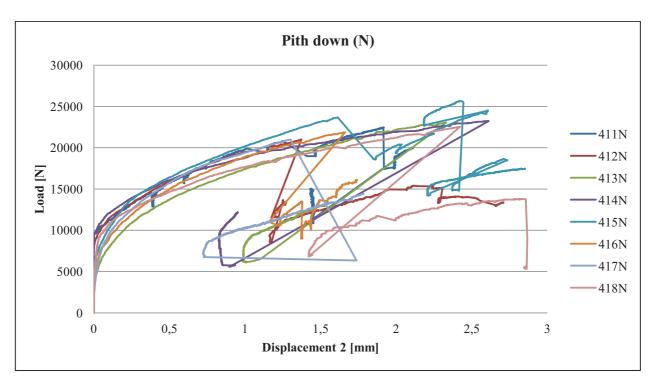


Figure 26: Load vs. displacement curves of bottom rail with pith down of Series 4 – Set 1. 8 failure mode of type 1

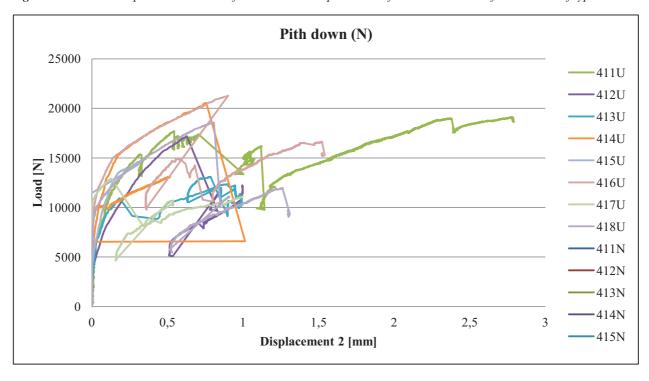


Figure 27: Load vs. displacement curves of bottom rail with pith up of Series 4 – Set 1. 8 failure mode of type1

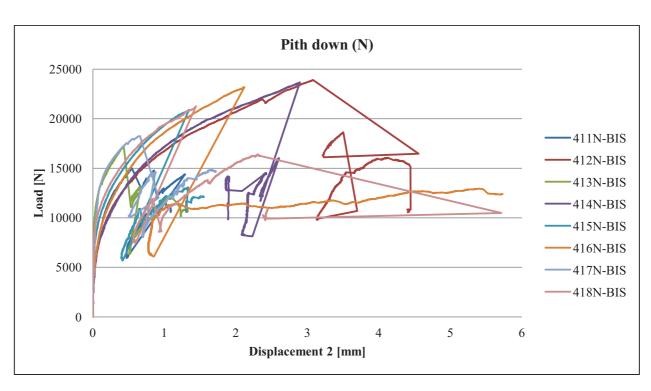


Figure 28: Load vs. displacement curves of bottom rail with pith down of Series 4 – Set 1-BIS. 8 failure mode of type 1

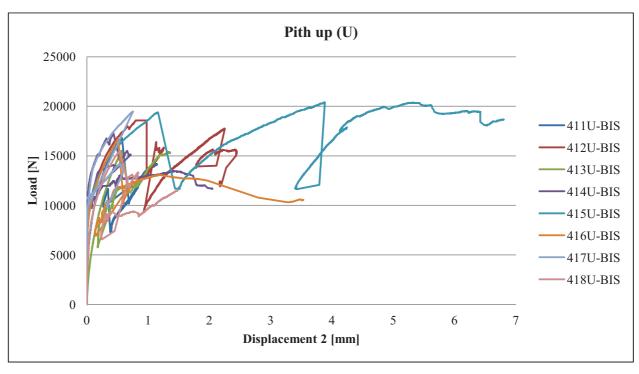


Figure 29: Load vs. displacement curves of bottom rail with pith up of Series 4 – Set 1-BIS. 8 failure mode of type 1

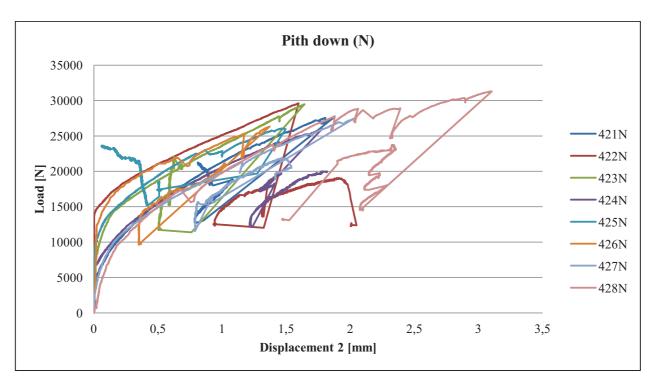


Figure 30: Load vs. displacement curves of bottom rail with pith down of Series 4 – Set 2. 8 failure mode of type 1

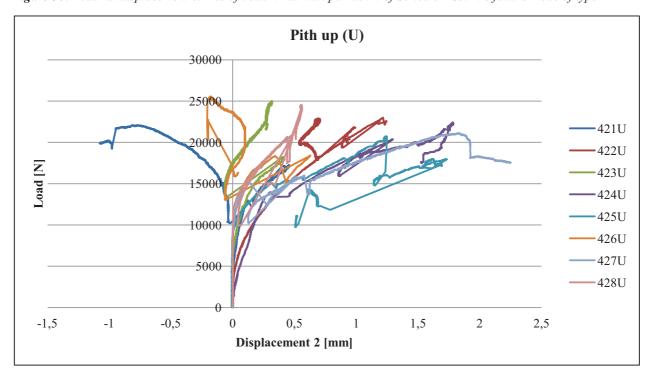


Figure 31: Load vs. displacement curves of bottom rail with pith up of Series 4 – Set 2. 8 failure mode of type 1

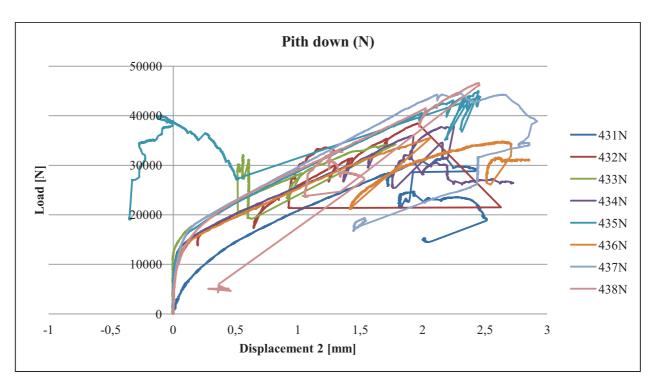


Figure 32: Load vs. displacement curves of bottom rail with pith down of Series 4 – Set 3. 6 failure mode of type 1 and 2 failure mode of type 2

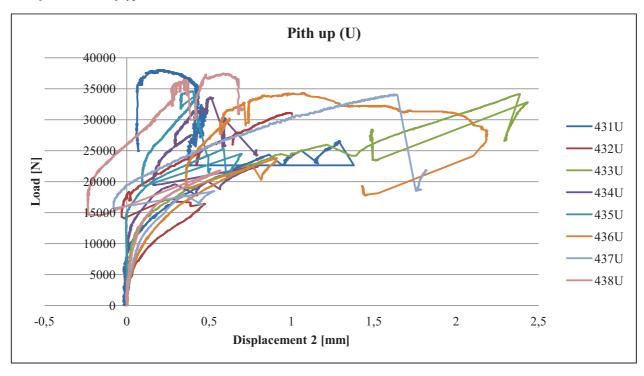


Figure 33: Load vs. displacement curves of bottom rail with pith up of Series 4 – Set 3. 8 failure mode of type 1

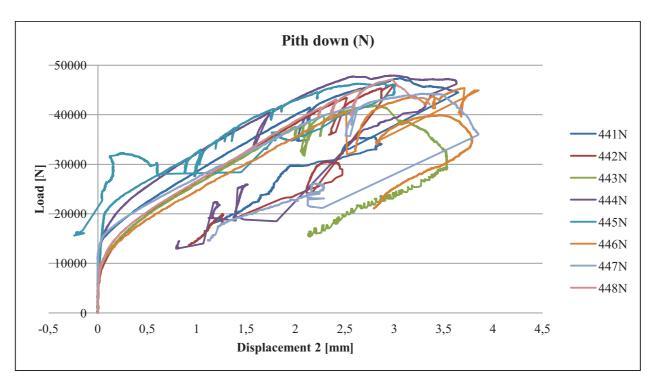


Figure 34: Load vs. displacement curves of bottom rail with pith down of Series 4 – Set 4. 1 failure mode of type 1, 4 failure mode of type 2 and 3 failure mode of type 3

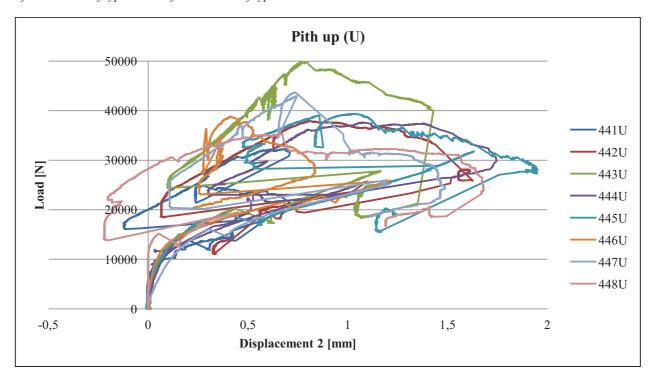


Figure 35: Load vs. displacement curves of bottom rail with pith up of Series 4 – Set 4. 8 failure mode of type 1 (see Appendix B notes $^{(1),(2)}$ and $^{(3)}$ about the type of failure of this set)

Summary of test results

The tables below summarize the average results from the tests for each set. Failure load, displacements at failure, edge of the bottom rail to fracture line distance as well as the density and the moisture content of the bottom rail are shown in relation to the pith orientation.

Series 4 – Anchor bolt at centre, 60 mm from the sheathing

Set 1 – Washer size 40x40 mm, distance from sheathing to edge of washer 40 mm

Pith Up - 8 tests

Table 3: Summary of test results for series 4 – set 1 – pith up

| | Failure load | Min. and max. failure load | Movement of washer surface on the side 1 in line of the anchor bolt | Movement of rail surface in line of the anchor bolt at centre of the rail | Density | Moisture |
|------------------|-----------------|-------------------------------------|---|---|----------------------|----------|
| | [kN] | [kN] | [mm] | [mm] | [kg/m ³] | [%] |
| Average | 16.8 | 10.9 ÷ 21.3 | 0.01 | 0.54 | 436.0 | 13.3 |
| St. Dev. | 3.65 | | - | - | 41.9 | 0.83 |
| Coeff. of Var. | 21.8 | - | - | - | 9.61 | 6.26 |
| [%] | | | | | | |
| Char. Value 0.05 | 8.80 | _ | _ | - | 344.6 | 11.5 |

| | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at the end on side 2 | Distance from edge of bottom rail to crack at anchor bolt 1 | Distance from edge of bottom rail to crack at anchor bolt 2 | |
|------------------|---|---|--|--|--|
| | [mm] | [mm] | [mm] | [mm] | |
| Average | 56.9 | 69.1 | 58.4 | 67.6 | |
| St. Dev. | 7.26 | 9.73 | 4.37 | 9.78 | |
| Coeff. of Var. | 12.8 | 14.1 | 7.49 | 14.5 | |
| [%] | | | | | |
| Char. Value 0.05 | 41.1 | 47.9 | 48.8 | 46.3 | |

⁸ failure mode of type 1

Pith Down - 8 tests

Table 4: Summary of test results for series 4 – set 1 – pith down

| | Failure load | Min. and max. failure load | Movement of washer surface on the side 1 in line of the anchor bolt [mm] | Movement of rail surface in line of the anchor bolt at centre of the rail [mm] | Density [kg/m³] | Moisture |
|------------------|-----------------|-------------------------------------|--|--|-----------------|----------|
| Average | 22.4 | 21.0 ÷ 23.7 | -0.03 | 1.90 | 414.4 | 13.0 |
| St. Dev. | 1.00 | - | - | - | 42.0 | 0.78 |
| Coeff. of Var. | 4.46 | - | - | - | 10.1 | 6.05 |
| [%] | | | | | | |
| Char. Value 0.05 | 20.2 | _ | _ | - | 322.8 | 11.3 |

| | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at anchor bolt 1 | Distance from edge of bottom rail to crack at anchor bolt 2 |
|------------------|---|---|--|--|
| | [mm] | [mm] | [mm] | [mm] |
| Average | 67.3 | 57.6 | 64.3 | 61.9 |
| St. Dev. | 15.3 | 10.6 | 15.9 | 13.0 |
| Coeff. of Var. | 22.7 | 18.4 | 24.8 | 21.0 |
| [%] | | | | |
| Char. Value 0.05 | 33.9 | 34.5 | 29.5 | 33.6 |

⁸ failure mode of type 1

Set 1-BIS – Washer size 40x40 mm, distance from sheathing to edge of washer 40 mm

Pith Up - 8 tests

Table 5: Summary of test results for series 4 – set 1-BIS – pith up

| | Failure load | Min. and max. failure load | Movement of washer surface on the side 1 in line of the anchor bolt [mm] | Movement of rail surface in line of the anchor bolt at centre of the rail [mm] | Density [kg/m³] | Moisture |
|------------------|-----------------|-------------------------------------|--|--|-----------------|----------|
| Average | 17.5 | 15.6 ÷ 19.5 | 0.03 | 0.69 | 412.4 | 13.6 |
| St. Dev. | 1.58 | - | - | - | 42.2 | 0.39 |
| Coeff. of Var. | 9.04 | - | - | - | 10.2 | 2.84 |
| [%] | | | | | | |
| Char. Value 0.05 | 14.0 | - | _ | - | 320.4 | 12.7 |

| | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at the end on side 2 | Distance from edge of bottom rail to crack at anchor bolt 1 | Distance from edge of bottom rail to crack at anchor bolt 2 |
|------------------|---|---|--|--|
| | [mm] | [mm] | [mm] | [mm] |
| Average | 46.8 | 64.9 | 50.8 | 59.1 |
| St. Dev. | 8.15 | 4.67 | 8.83 | 3.36 |
| Coeff. of Var. | 17.4 | 7.20 | 17.4 | 5.68 |
| [%] | | | | |
| Char. Value 0.05 | 29.0 | 54.7 | 31.5 | 51.8 |

⁸ failure mode of type 1

Pith Down - 8 tests

Table 6: Summary of test results for series 4 – set 1-BIS – pith down

| | Failure load | Min. and max. failure load | Movement of washer surface on the side 1 in line of the anchor bolt [mm] | Movement of rail surface in line of the anchor bolt at centre of the rail [mm] | Density [kg/m³] | Moisture |
|------------------|-----------------|-------------------------------------|--|--|-----------------|----------|
| Average | 20.4 | 15.0 ÷ 24.0 | 0.01 | 1.56 | 404.1 | 13.4 |
| St. Dev. | 3.29 | - | - | - | 29.4 | 0.36 |
| Coeff. of Var. | 16.1 | - | - | - | 7.27 | 2.70 |
| Char. Value 0.05 | 13.3 | - | - | - | 340.0 | 12.6 |

| | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at anchor bolt 1 | Distance from edge of bottom rail to crack at anchor bolt 2 |
|------------------|---|---|--|--|
| | [mm] | [mm] | [mm] | [mm] |
| Average | 68.0 | 45.0 | 65.4 | 47.5 |
| St. Dev. | 12.6 | 9.64 | 12.6 | 8.80 |
| Coeff. of Var. | 18.5 | 21.4 | 19.2 | 18.5 |
| [%] | | | | |
| Char. Value 0.05 | 40.6 | 24.0 | 38.0 | 28.3 |

⁸ failure mode of type 1

Set 2- Washer size 60x60 mm, distance from sheathing to edge of washer 30 mm

Pith Up - 8 tests

Table 7: Summary of test results for series 4 – set 2 – pith up

| | Failure load | Min. and max. failure load | Movement of washer surface on the side 1 in line of the anchor bolt [mm] | Movement of rail surface in line of the anchor bolt at centre of the rail [mm] | Density [kg/m³] | Moisture |
|------------------|-----------------|-------------------------------------|--|--|-----------------|----------|
| Average | 19.3 | 15.2 ÷ 23.0 | -0.01 | 0.74 | 424.4 | 12.7 |
| St. Dev. | 2.49 | - | - | - | 60.5 | 0.95 |
| Coeff. of Var. | 12.9 | - | - | - | 14.3 | 7.52 |
| [%] | | | | | | |
| Char. Value 0.05 | 13.9 | - | - | - | 292.4 | 10.6 |

| | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at the end on side 2 | Distance from edge of bottom rail to crack at anchor bolt 1 | Distance from edge of bottom rail to crack at anchor bolt 2 |
|------------------|---|---|--|---|
| | [mm] | [mm] | [mm] | [mm] |
| Average | 60.0 | 68.4 | 61.6 | 67.6 |
| St. Dev. | 9.35 | 16.5 | 9.09 | 15.3 |
| Coeff. of Var. | 15.6 | 24.1 | 14.7 | 22.6 |
| [%] | | | | |
| Char. Value 0.05 | 39.6 | 32.5 | 41.8 | 34.4 |

⁸ failure mode of type 1

Pith Down - 8 tests

Table 8: Summary of test results for series 4 – set 2 – pith down

| | Failure load | Min. and max. failure load | Movement of washer surface on the side 1 in line of the anchor bolt [mm] | Movement of rail surface in line of the anchor bolt at centre of the rail [mm] | Density [kg/m³] | Moisture |
|------------------|-----------------|-------------------------------------|--|--|-----------------|----------|
| Average | 28.0 | 26.1 ÷ 31.3 | 0.01 | 1.86 | 403.6 | 13.1 |
| St. Dev. | 1.94 | - | - | - | 29.8 | 0.64 |
| Coeff. of Var. | 6.94 | - | - | - | 7.38 | 4.89 |
| [%] | | | | | | |
| Char. Value 0.05 | 23.8 | - | - | - | 338.7 | 11.7 |

| | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at anchor bolt 1 | Distance from edge of bottom rail to crack at anchor bolt 2 |
|------------------|---|---|--|--|
| | [mm] | [mm] | [mm] | [mm] |
| Average | 70.9 | 50.1 | 67.6 | 53.9 |
| St. Dev. | 16.4 | 8.15 | 13.7 | 8.36 |
| Coeff. of Var. | 23.1 | 16.3 | 20.3 | 15.5 |
| [%] | | | | |
| Char. Value 0.05 | 35.1 | 32.4 | 37.7 | 35.7 |

⁸ failure mode of type 1

Set 3 – Washer size 80x70 mm, distance from sheathing to edge of washer 20 mm

Pith Up - 8 tests

Table 9: Summary of test results for series 4 – set 3 – pith up

| | Failure load | Min. and max. failure load | Movement of washer surface on the side 1 in line of the anchor bolt [mm] | Movement of rail surface in line of the anchor bolt at centre of the rail [mm] | Density [kg/m³] | Moisture |
|------------------|-----------------|-------------------------------------|--|--|-----------------|----------|
| Average | 23.7 | 17.2 ÷ 34.1 | 0.02 | 0.92 | 426.6* | 13.1* |
| St. Dev. | 5.27 | - | - | - | 40.2 | 1.11 |
| Coeff. of Var. | 22.2 | - | - | - | 9.41 | 8.51 |
| [%] | | | | | | |
| Char. Value 0.05 | 12.2 | _ | - | - | 336.7 | 10.6 |

| | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at anchor bolt 1 | Distance from edge of bottom rail to crack at anchor bolt 2 |
|------------------|---|---|--|---|
| | [mm] | [mm] | [mm] | [mm] |
| Average | 52.9 | 68.8 | 56.3 | 67.1 |
| St. Dev. | 9.86 | 11.9 | 10.7 | 8.98 |
| Coeff. of Var. | 18.7 | 17.3 | 18.9 | 13.4 |
| [%] | | | | |
| Char. Value 0.05 | 31.4 | 42.9 | 33.0 | 47.5 |

^{*}data available for seven tests

⁸ failure mode of type 1

Pith Down - 8 tests

Table 10: Summary of test results for series 4 – set 3 – pith down

| | Failure load | Min. and max. failure load | Movement of washer surface on the side 1 in line of the anchor bolt [mm] | Movement of rail surface in line of the anchor bolt at centre of the rail [mm] | Density [kg/m³] | Moisture |
|-------------------------|-----------------|-------------------------------------|--|--|-----------------|----------|
| Average | 38.4 | 28.4 ÷ 46.6 | 0.07 | 2.08 | 441.1 | 13.2 |
| St. Dev. | 6.46 | - | - | - | 45.2 | 1.23 |
| Coeff. of Var. | 16.8 | - | - | - | 10.2 | 9.37 |
| [%] Char. Value 0.05 | 24.3 | - | - | - | 342.6 | 10.5 |

| | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at anchor bolt 1 | Distance from edge of bottom rail to crack at anchor bolt 2 |
|------------------|---|---|--|--|
| | [mm] | [mm] | [mm] | [mm] |
| Average | 66.3* | 46.7* | 63.2* | 54.2* |
| St. Dev. | 27.2 | 19.7 | 25.9 | 22.0 |
| Coeff. of Var. | 41.0 | 42.3 | 41.0 | 40.6 |
| [%] | | | | |
| Char. Value 0.05 | 2.92 | 0.73 | 2.90 | 2.98 |

^{*}data available for six tests

 $^{6\} failure\ mode\ of\ type\ 1\ and\ 2\ of\ type\ 2$

Set 4- Washer size 100x70 mm, distance from sheathing to edge of washer 10 mm

Pith Up - 8 tests

Table 11: Summary of test results for series 4 – set 4 – pith up

| | Failure load | Min. and max. failure load | Movement of washer surface on the side 1 in line of the anchor bolt [mm] | Movement of rail surface in line of the anchor bolt at centre of the rail [mm] | Density [kg/m³] | Moisture |
|------------------|-----------------|-------------------------------------|--|--|-----------------|----------|
| Average | 20.0 | 13.8 ÷ 25.9 | 0.04 | 0.60 | 410.3 | 12.0 |
| St. Dev. | 4.80 | - | - | - | 34.1 | 1.41 |
| Coeff. of Var. | 23.9 | - | - | - | 8.32 | 11.8 |
| [%] | | | | | | |
| Char. Value 0.05 | 9.59 | _ | - | - | 335.9 | 8.89 |

| | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at the end on side 2 | Distance from edge of bottom rail to crack at anchor bolt 1 | Distance from edge of bottom rail to crack at anchor bolt 2 |
|------------------|---|---|--|--|
| | [mm] | [mm] | [mm] | [mm] |
| Average | 49.6 | 61.4 | 53.5 | 60.0 |
| St. Dev. | 14.0 | 4.14 | 11.7 | 1.41 |
| Coeff. of Var. | 28.2 | 6.74 | 21.8 | 2.36 |
| [%] | | | | |
| Char. Value 0.05 | 19.2 | 52.4 | 28.1 | 56.9 |

⁸ failure mode of type 1 (see Appendix B notes (1), (2) and (3) about the type of failure of this set)

Pith Down - 8 tests

Table 12: Summary of test results for series 4 – set 4 – pith down

| | Failure load | Min. and max. failure load | Movement of washer surface on the side 1 in line of the anchor bolt [mm] | Movement of rail surface in line of the anchor bolt at centre of the rail [mm] | Density [kg/m³] | Moisture |
|------------------|-----------------|-------------------------------------|--|--|-----------------|----------|
| Average | 45.8 | 41.9 ÷ 48.0 | 0.15 | 3.10 | 398.8 | 12.2 |
| St. Dev. | 1.97 | - | - | - | 16.8 | 1.07 |
| Coeff. of Var. | 4.31 | - | - | - | 4.22 | 8.70 |
| [%] | | | | | | |
| Char. Value 0.05 | 41.5 | - | - | - | 362.1 | 9.92 |

| | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at the end on side | Distance from edge of bottom rail to crack at anchor bolt 1 | Distance from edge of bottom rail to crack at anchor bolt 2 |
|------------------|---|---|--|---|
| | [mm] | [mm] | [mm] | [mm] |
| Average | 50.0* | 24.0* | 54.0* | 17.0* |
| St. Dev. | - | - | - | - |
| Coeff. of Var. | - | - | - | - |
| [%] | | | | |
| Char. Value 0.05 | - | - | - | - |

^{*}data available only for the specimen 446N, the only one with failure mode of type 1

¹ failure mode of type 1, 4 failure mode of type 2 and 3 failure mode of type 3

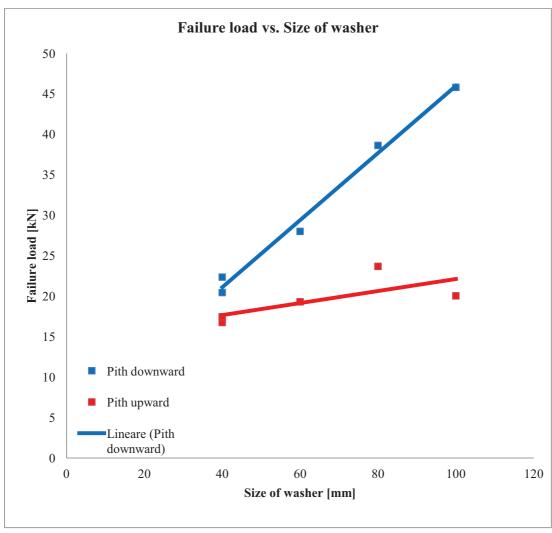


Figure 36: Failure load vs. size of washer of bottom rail with pith upward and pith downward

Summary of failure load

Table 13: Summary of failure load results for each set

| Washer size | Average of failure load Pith up | Average of failure load Pith down | Figure of reference | Ratio between Pith up and Pith down failure |
|-------------|---------------------------------------|-----------------------------------|---------------------|---|
| [mm] | [kN] | [kN] | | load |
| 40x40 | 16.8 | 22.4 | Fig. 7 and 8 | 0.75 |
| 40x40 - Bis | 17.5 | 20.4 | Fig. 9 and 10 | 0.86 |
| 60x60 | 19.3 | 28.0 | Fig. 7 and 8 | 0.69 |
| 80x70 | 23.7 | 38.4 | Fig. 7 and 8 | 0.62 |
| 100x70 | 20.0 | 45.8 | Fig. 7 and 8 | 0.44 |

Conclusions

The test results show that the size of the washer has a significant influence on the failure load and the failure modes. Moreover the results show that the orientation of the pith also has a significant influence on the failure load.

Three primary failure modes were found during the tests:

- failure mode 1: due to splitting of the underneath side of the bottom rail. This brittle type
 of failure occurs when medium sized washers are used with large distance to the loaded
 edge of the bottom rail;
- failure mode 2: due to splitting at the edge side of the bottom rail. This type of failure occurs when is decreased the distance between the edge of the washer and the edge of the bottom rail;
- failure mode 3: due to plastic bending and pull-out of nails (and therefore a detachment of the sheathing). This failure mode was not planned (the test series were planned so that splitting would occur), but happened when there was not splitting of the bottom rail due to large anchor bolts and small distance between the edge of the washer and the edge of the bottom rail.

It was found that decreasing the distance between the edge of the washer and the edge of the bottom rail increases the maximum load.

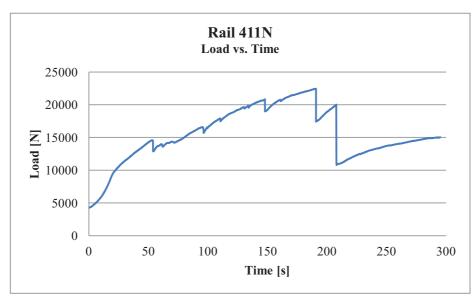
It was also observed that most the failure mode 1 (splitting of the underneath surface of the bottom rail) appears independently on either end of the bottom rail and sometime simultaneously on both length-wise ends of the bottom rail.

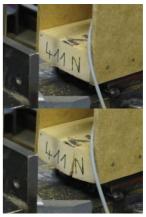
Appendix A

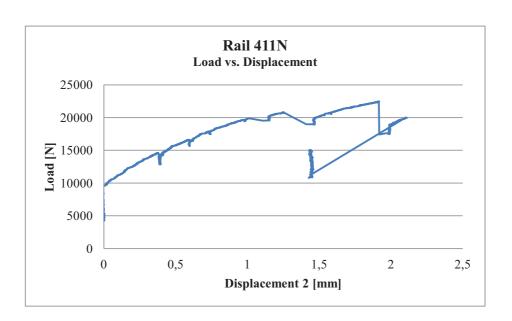
Series 4 – Anchor bolt at centre, 60 mm from the sheathing

Set 1 – Size of washer 40x40 mm

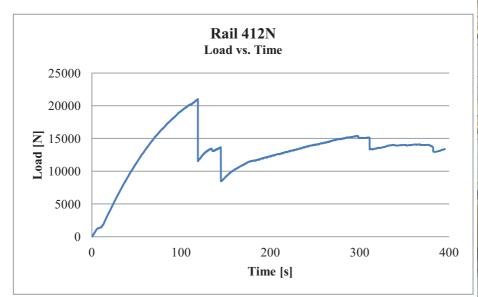
Pith Down



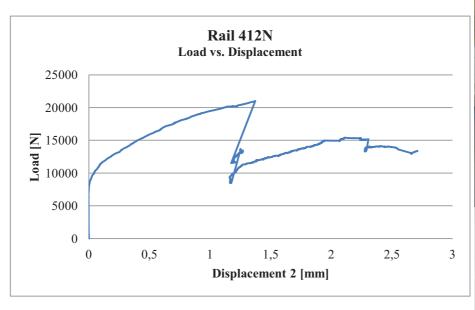




| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 22451 |
| Displacement 1 at failure [mm] | 0,10 |
| Displacement 2 at failure [mm] | 1,91 |
| Distance from crack to edge side 1 [mm] | 50 |
| Distance from crack to edge side 2 [mm] | 72 |
| Distance from crack to anchor bolt side 1 [mm] | 45 |
| Distance from crack to anchor bolt side 2 [mm] | 83 |
| Moisture [%] | 11,8 |
| Dry density [kg/m ³] | 406 |

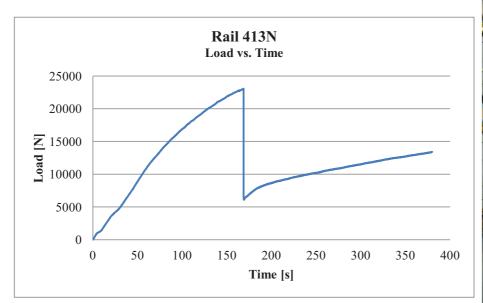




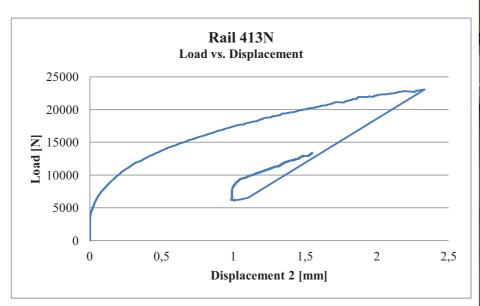




| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 21010 |
| Displacement 1 at failure [mm] | -0,02 |
| Displacement 2 at failure [mm] | 1,37 |
| Distance from crack to edge side 1 [mm] | 90 |
| Distance from crack to edge side 2 [mm] | 52 |
| Distance from crack to anchor bolt side 1 [mm] | 85 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 14,3 |
| Dry density [kg/m ³] | 462 |

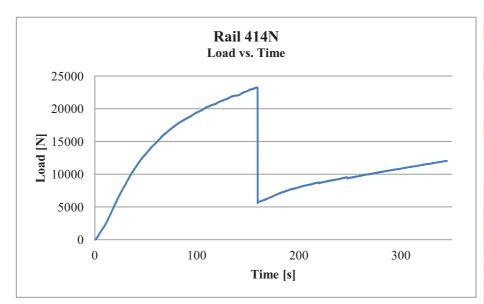




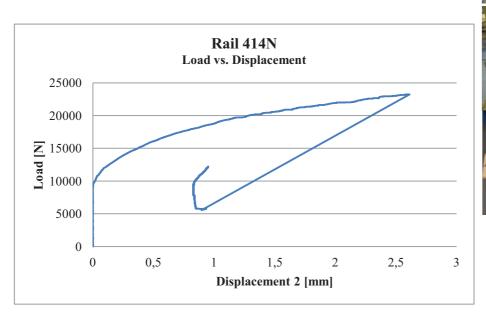




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 23057 |
| Displacement 1 at failure [mm] | -0,09 |
| Displacement 2 at failure [mm] | 2,33 |
| Distance from crack to edge side 1 [mm] | 60 |
| Distance from crack to edge side 2 [mm] | 54 |
| Distance from crack to anchor bolt side 1 [mm] | 55 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 12,4 |
| Dry density [kg/m ³] | 389 |

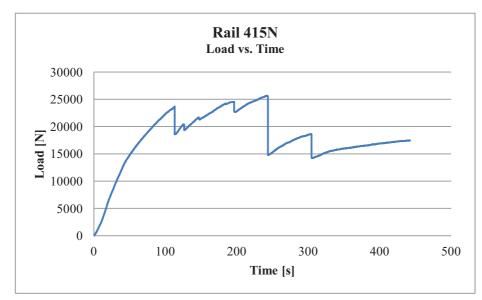




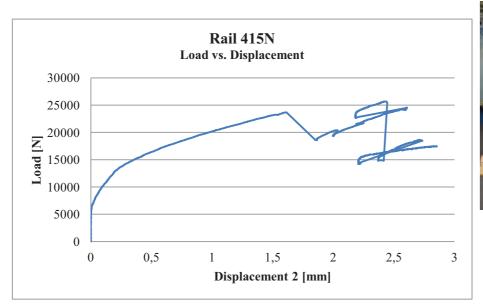




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 23240 |
| Displacement 1 at failure [mm] | -0,01 |
| Displacement 2 at failure [mm] | 2,61 |
| Distance from crack to edge side 1 [mm] | 65 |
| Distance from crack to edge side 2 [mm] | 57 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,0 |
| Dry density [kg/m ³] | 338 |

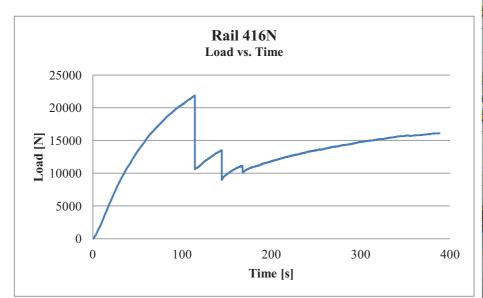




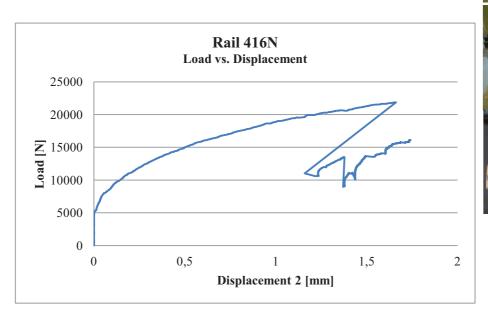




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 23676 |
| Displacement 1 at failure [mm] | -0,04 |
| Displacement 2 at failure [mm] | 1,61 |
| Distance from crack to edge side 1 [mm] | 63 |
| Distance from crack to edge side 2 [mm] | 60 |
| Distance from crack to anchor bolt side 1 [mm] | 66 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 12,8 |
| Dry density [kg/m ³] | 449 |

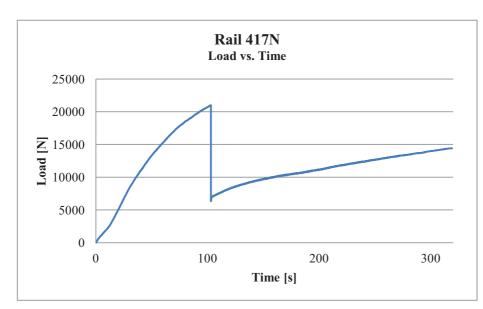


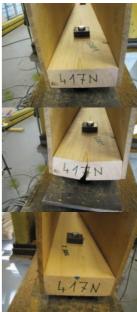


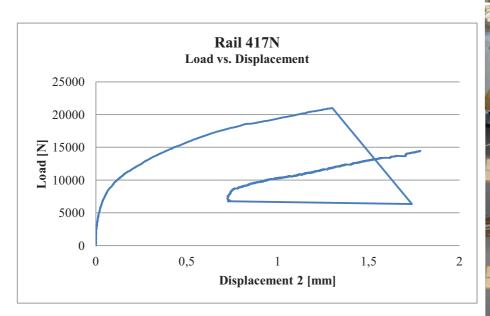




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 21866 |
| Displacement 1 at failure [mm] | -0,02 |
| Displacement 2 at failure [mm] | 1,66 |
| Distance from crack to edge side 1 [mm] | 65 |
| Distance from crack to edge side 2 [mm] | 40 |
| Distance from crack to anchor bolt side 1 [mm] | 59 |
| Distance from crack to anchor bolt side 2 [mm] | 44 |
| Moisture [%] | 13,6 |
| Dry density [kg/m ³] | 443 |

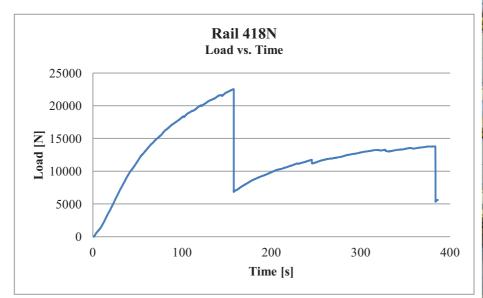




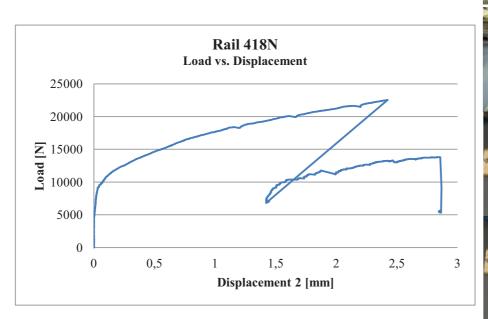




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 20995 |
| Displacement 1 at failure [mm] | -0,01 |
| Displacement 2 at failure [mm] | 1,30 |
| Distance from crack to edge side 1 [mm] | 54 |
| Distance from crack to edge side 2 [mm] | 54 |
| Distance from crack to anchor bolt side 1 [mm] | 53 |
| Distance from crack to anchor bolt side 2 [mm] | 50 |
| Moisture [%] | 12,3 |
| Dry density [kg/m ³] | 442 |



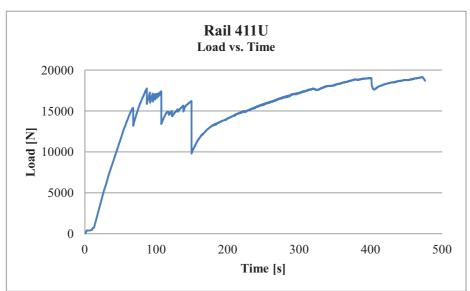




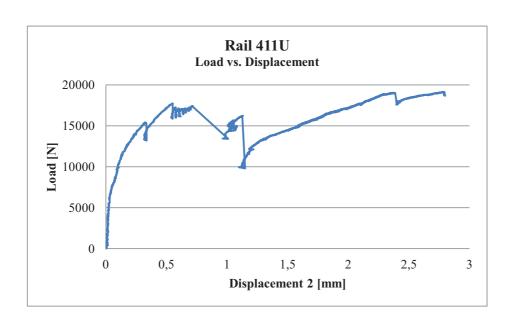


| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 22532 |
| Displacement 1 at failure [mm] | -0,20 |
| Displacement 2 at failure [mm] | 2,42 |
| Distance from crack to edge side 1 [mm] | 91 |
| Distance from crack to edge side 2 [mm] | 72 |
| Distance from crack to anchor bolt side 1 [mm] | 91 |
| Distance from crack to anchor bolt side 2 [mm] | 78 |
| Moisture [%] | 13,2 |
| Dry density [kg/m ³] | 386 |

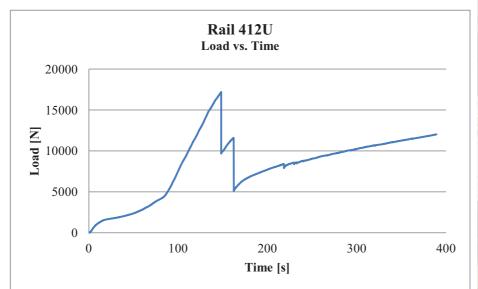
Pith Up

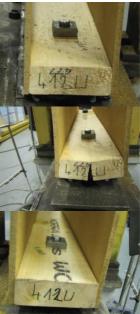


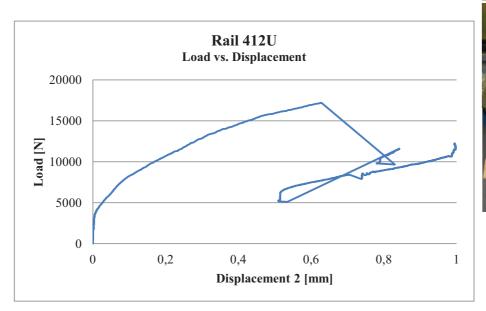




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 17745 |
| Displacement 1 at failure [mm] | 0,01 |
| Displacement 2 at failure [mm] | 0,55 |
| Distance from crack to edge side 1 [mm] | 52 |
| Distance from crack to edge side 2 [mm] | 65 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 12,4 |
| Dry density [kg/m ³] | 443 |

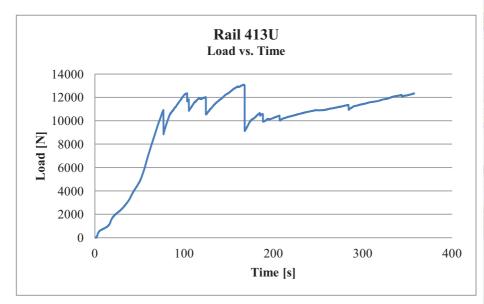




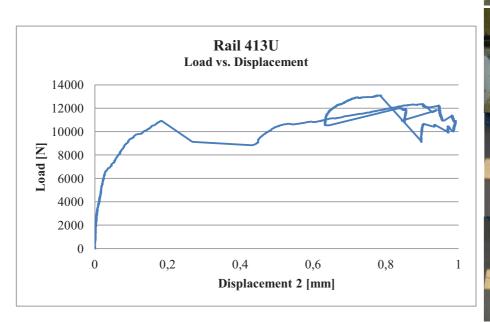




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 17193 |
| Displacement 1 at failure [mm] | 0,06 |
| Displacement 2 at failure [mm] | 0,63 |
| Distance from crack to edge side 1 [mm] | 59 |
| Distance from crack to edge side 2 [mm] | 63 |
| Distance from crack to anchor bolt side 1 [mm] | 59 |
| Distance from crack to anchor bolt side 2 [mm] | 64 |
| Moisture [%] | 13,8 |
| Dry density [kg/m ³] | 445 |



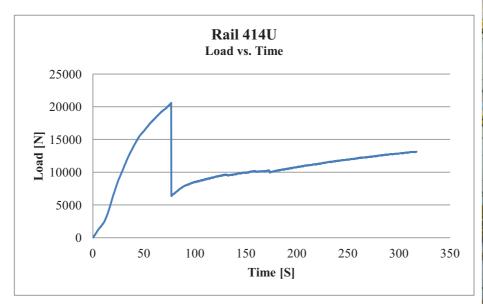




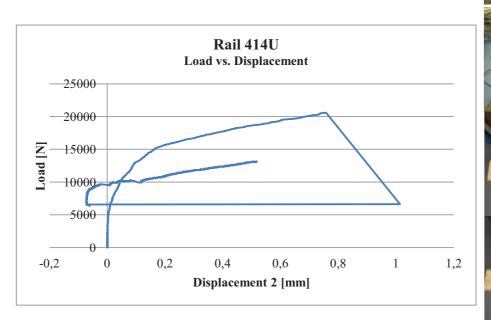


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 10922 |
| Displacement 1 at failure [mm] | -0,03 |
| Displacement 2 at failure [mm] | 0,18 |
| Distance from crack to edge side 1 [mm] | 70 |
| Distance from crack to edge side 2 [mm] | 58 |
| Distance from crack to anchor bolt side 1 [mm] | 58 |
| Distance from crack to anchor bolt side 2 [mm] | 65 |
| Moisture [%] | 13,2 |
| Dry density [kg/m ³] | 422 |

Probable influence of the pre-crack in the side 1.

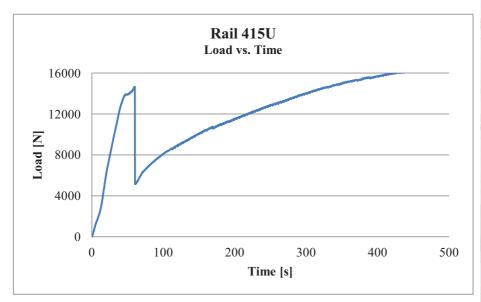




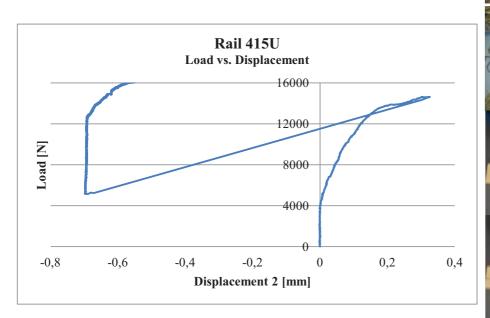




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 20589 |
| Displacement 1 at failure [mm] | 0,03 |
| Displacement 2 at failure [mm] | 0,76 |
| Distance from crack to edge side 1 [mm] | 53 |
| Distance from crack to edge side 2 [mm] | 85 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 83 |
| Moisture [%] | 14,7 |
| Dry density [kg/m ³] | 434 |



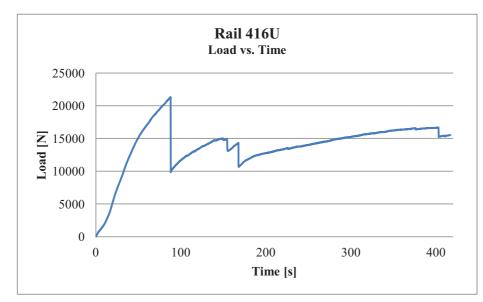




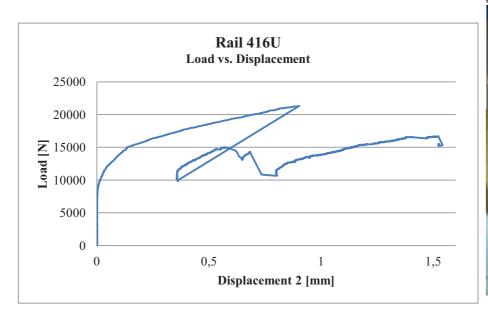


| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 14643 |
| Displacement 1 at failure [mm] | 0,02 |
| Displacement 2 at failure [mm] | 0,33 |
| Distance from crack to edge side 1 [mm] | 52 |
| Distance from crack to edge side 2 [mm] | 63 |
| Distance from crack to anchor bolt side 1 [mm] | 51 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,7 |
| Dry density [kg/m ³] | 523 |

Probable influence of the pre-crack in the side 2.

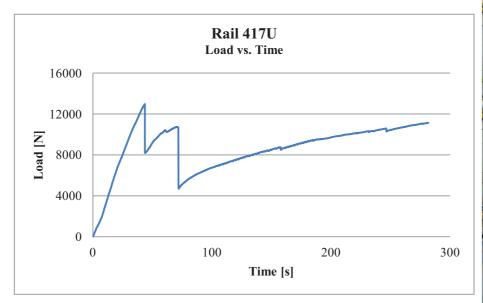




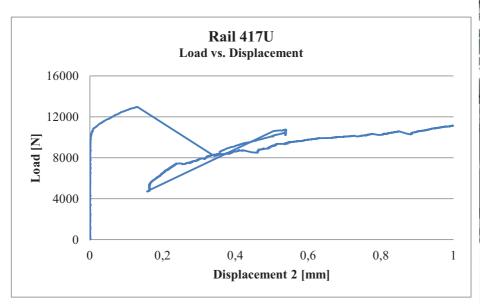




| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 21328 |
| Displacement 1 at failure [mm] | 0,03 |
| Displacement 2 at failure [mm] | 0,90 |
| Distance from crack to edge side 1 [mm] | 57 |
| Distance from crack to edge side 2 [mm] | 63 |
| Distance from crack to anchor bolt side 1 [mm] | 64 |
| Distance from crack to anchor bolt side 2 [mm] | 56 |
| Moisture [%] | 12,8 |
| Dry density [kg/m ³] | 435 |



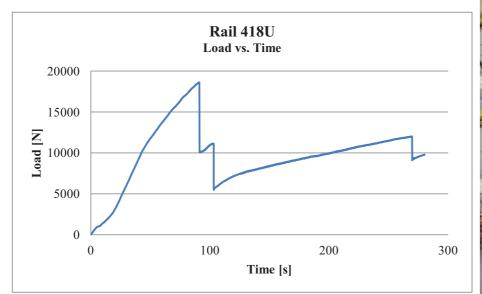




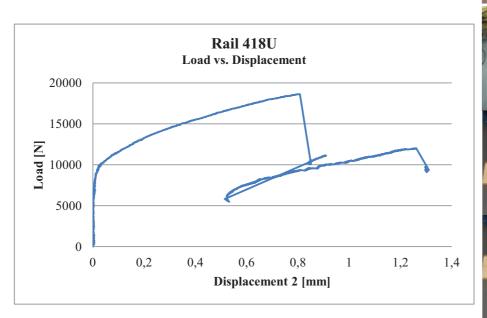


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 12972 |
| Displacement 1 at failure [mm] | -0,01 |
| Displacement 2 at failure [mm] | 0,13 |
| Distance from crack to edge side 1 [mm] | 48 |
| Distance from crack to edge side 2 [mm] | 78 |
| Distance from crack to anchor bolt side 1 [mm] | 53 |
| Distance from crack to anchor bolt side 2 [mm] | 75 |
| Moisture [%] | 13,1 |
| Dry density [kg/m ³] | 374 |

Possible pre-crack on the side 1.





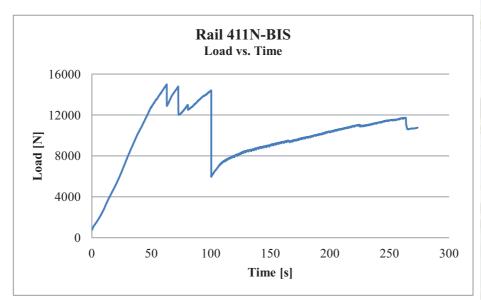




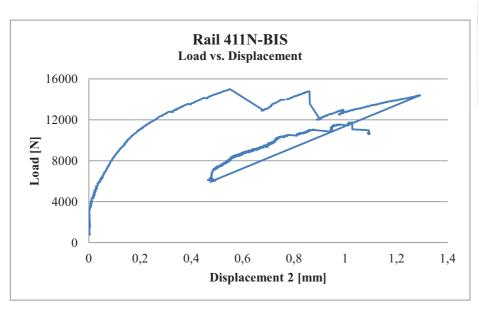
| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 18612 |
| Displacement 1 at failure [mm] | -0,02 |
| Displacement 2 at failure [mm] | 0,80 |
| Distance from crack to edge side 1 [mm] | 64 |
| Distance from crack to edge side 2 [mm] | 78 |
| Distance from crack to anchor bolt side 1 [mm] | 62 |
| Distance from crack to anchor bolt side 2 [mm] | 78 |
| Moisture [%] | 12,2 |
| Dry density [kg/m ³] | 411 |

Set 1-BIS – Size of washer 40x40 mm

Pith down

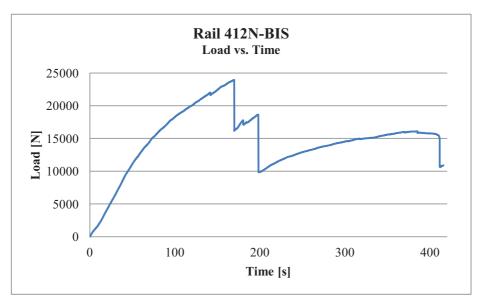




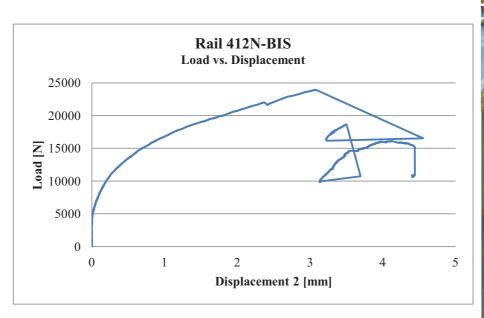




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 14987 |
| Displacement 1 at failure [mm] | 0,00 |
| Displacement 2 at failure [mm] | 0,55 |
| Distance from crack to edge side 1 [mm] | 53 |
| Distance from crack to edge side 2 [mm] | 40 |
| Distance from crack to anchor bolt side 1 [mm] | 54 |
| Distance from crack to anchor bolt side 2 [mm] | 39 |
| Moisture [%] | 13,8 |
| Dry density [kg/m ³] | 357 |

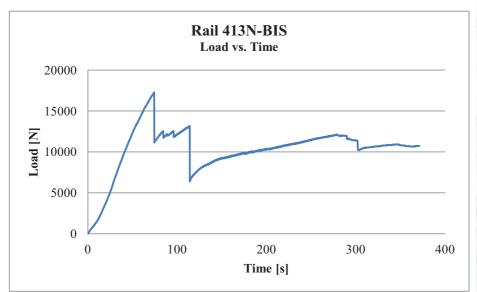




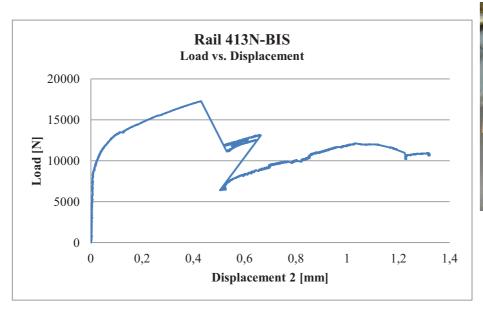




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 23952 |
| Displacement 1 at failure [mm] | 0,02 |
| Displacement 2 at failure [mm] | 3,08 |
| Distance from crack to edge side 1 [mm] | 84 |
| Distance from crack to edge side 2 [mm] | 40 |
| Distance from crack to anchor bolt side 1 [mm] | 85 |
| Distance from crack to anchor bolt side 2 [mm] | 55 |
| Moisture [%] | 13,8 |
| Dry density [kg/m ³] | 369 |

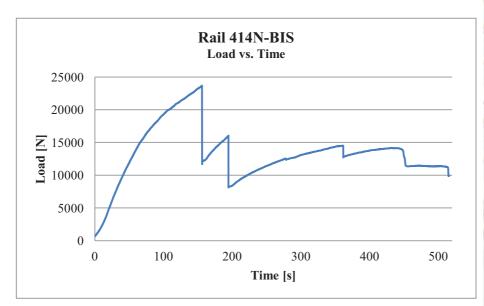




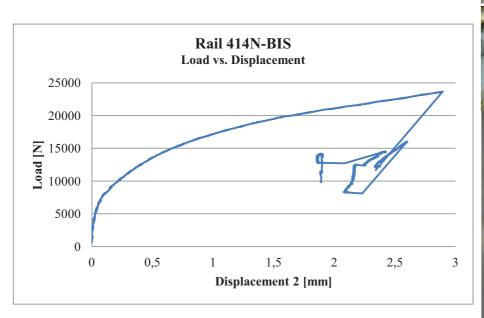




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 17263 |
| Displacement 1 at failure [mm] | -0,03 |
| Displacement 2 at failure [mm] | 0,43 |
| Distance from crack to edge side 1 [mm] | 59 |
| Distance from crack to edge side 2 [mm] | 44 |
| Distance from crack to anchor bolt side 1 [mm] | 59 |
| Distance from crack to anchor bolt side 2 [mm] | 44 |
| Moisture [%] | 12,9 |
| Dry density [kg/m ³] | 410 |

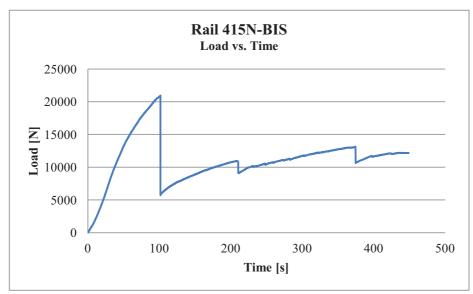




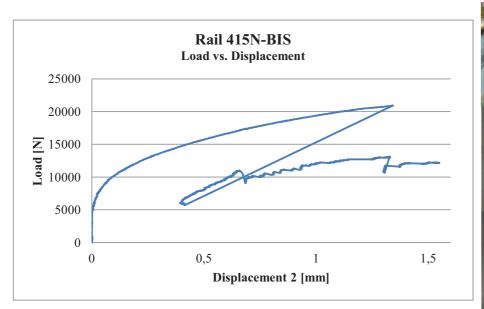




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 23682 |
| Displacement 1 at failure [mm] | 0,01 |
| Displacement 2 at failure [mm] | 2,89 |
| Distance from crack to edge side 1 [mm] | 65 |
| Distance from crack to edge side 2 [mm] | 48 |
| Distance from crack to anchor bolt side 1 [mm] | 59 |
| Distance from crack to anchor bolt side 2 [mm] | 52 |
| Moisture [%] | 13,5 |
| Dry density [kg/m ³] | 433 |

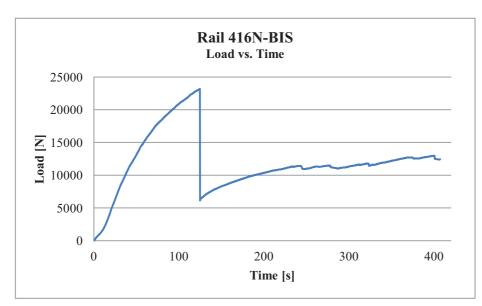




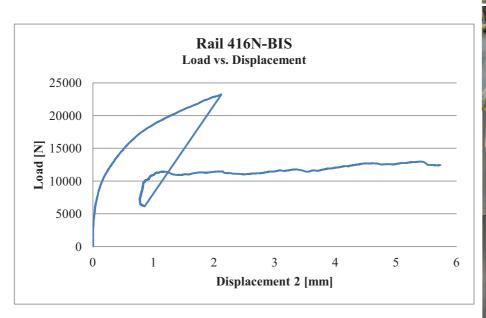




| Type of failure | Failure 1 – 1 st crack at side 1 |
|--|---|
| Failure load [N] | 20917 |
| Displacement 1 at failure [mm] | 0,00 |
| Displacement 2 at failure [mm] | 1,34 |
| Distance from crack to edge side 1 [mm] | 65 |
| Distance from crack to edge side 2 [mm] | 36 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 36 |
| Moisture [%] | 13,6 |
| Dry density [kg/m ³] | 393 |

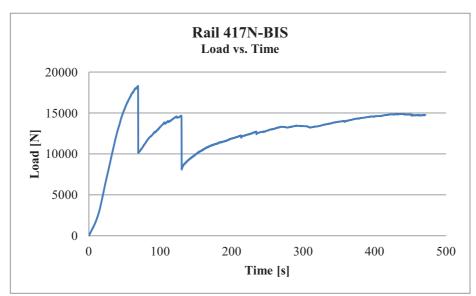




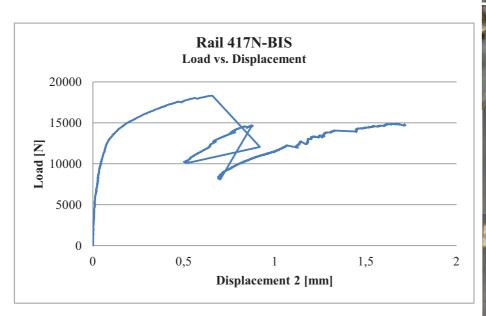




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 23217 |
| Displacement 1 at failure [mm] | 0,00 |
| Displacement 2 at failure [mm] | 2,12 |
| Distance from crack to edge side 1 [mm] | 62 |
| Distance from crack to edge side 2 [mm] | 40 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 46 |
| Moisture [%] | 13,6 |
| Dry density [kg/m ³] | 433 |

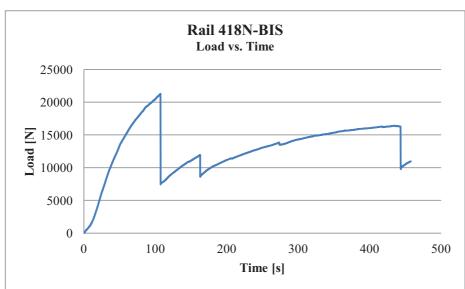




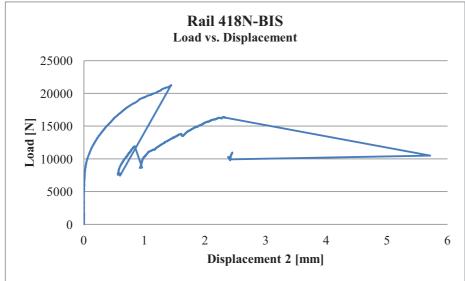




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 18293 |
| Displacement 1 at failure [mm] | 0,05 |
| Displacement 2 at failure [mm] | 0,65 |
| Distance from crack to edge side 1 [mm] | 66 |
| Distance from crack to edge side 2 [mm] | 45 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 45 |
| Moisture [%] | 13,2 |
| Dry density [kg/m ³] | 433 |



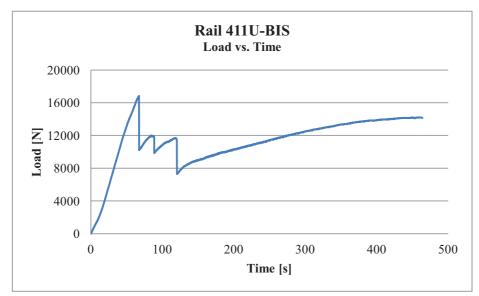




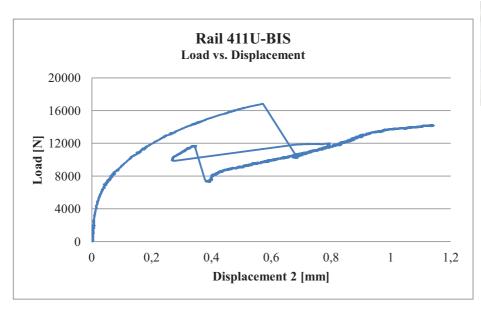


| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 21276 |
| Displacement 1 at failure [mm] | 0,03 |
| Displacement 2 at failure [mm] | 1,44 |
| Distance from crack to edge side 1 [mm] | 90 |
| Distance from crack to edge side 2 [mm] | 67 |
| Distance from crack to anchor bolt side 1 [mm] | 86 |
| Distance from crack to anchor bolt side 2 [mm] | 63 |
| Moisture [%] | 13,0 |
| Dry density [kg/m ³] | 404 |

Pith Up





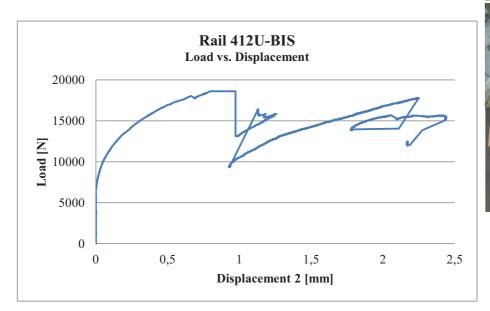




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 21276 |
| Displacement 1 at failure [mm] | 0,10 |
| Displacement 2 at failure [mm] | 0,57 |
| Distance from crack to edge side 1 [mm] | 58 |
| Distance from crack to edge side 2 [mm] | 67 |
| Distance from crack to anchor bolt side 1 [mm] | 61 |
| Distance from crack to anchor bolt side 2 [mm] | 62 |
| Moisture [%] | 14,0 |
| Dry density [kg/m ³] | 364 |

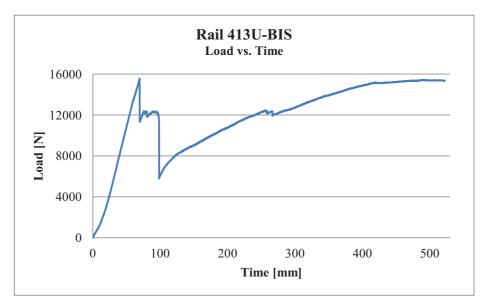




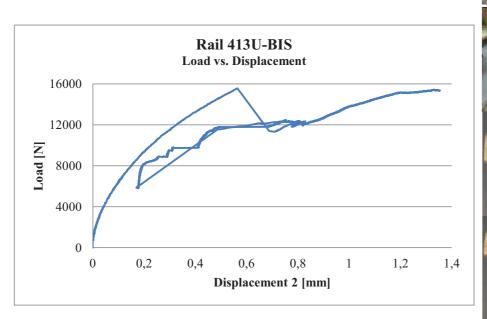




| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 18601 |
| Displacement 1 at failure [mm] | 0,09 |
| Displacement 2 at failure [mm] | 0,97 |
| Distance from crack to edge side 1 [mm] | 57 |
| Distance from crack to edge side 2 [mm] | 70 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,8 |
| Dry density [kg/m ³] | 396 |

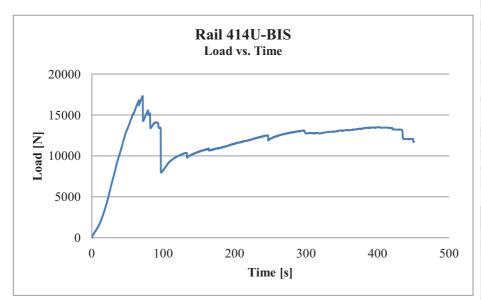




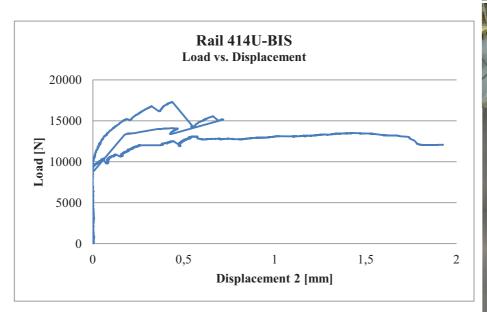




| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 15560 |
| Displacement 1 at failure [mm] | 0,01 |
| Displacement 2 at failure [mm] | 0,56 |
| Distance from crack to edge side 1 [mm] | 44 |
| Distance from crack to edge side 2 [mm] | 64 |
| Distance from crack to anchor bolt side 1 [mm] | 46 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,7 |
| Dry density [kg/m ³] | 382 |

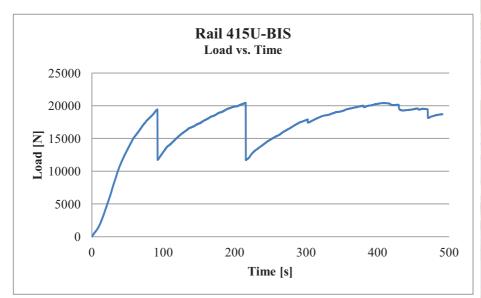




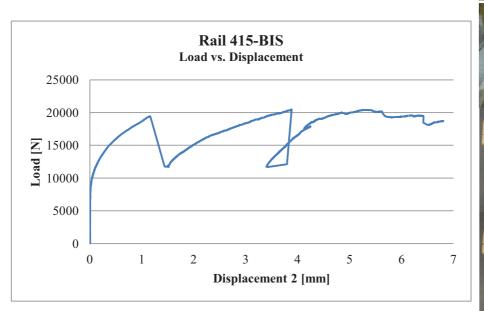




| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 17313 |
| Displacement 1 at failure [mm] | -0,01 |
| Displacement 2 at failure [mm] | 0,44 |
| Distance from crack to edge side 1 [mm] | 40 |
| Distance from crack to edge side 2 [mm] | 70 |
| Distance from crack to anchor bolt side 1 [mm] | 42 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,0 |
| Dry density [kg/m ³] | 503 |





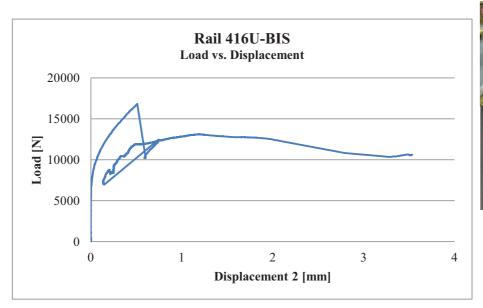




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 19426 |
| Displacement 1 at failure [mm] | 0,00 |
| Displacement 2 at failure [mm] | 1,16 |
| Distance from crack to edge side 1 [mm] | 50 |
| Distance from crack to edge side 2 [mm] | 67 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 14,0 |
| Dry density [kg/m ³] | 410 |

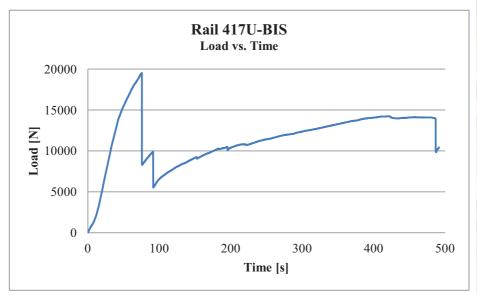




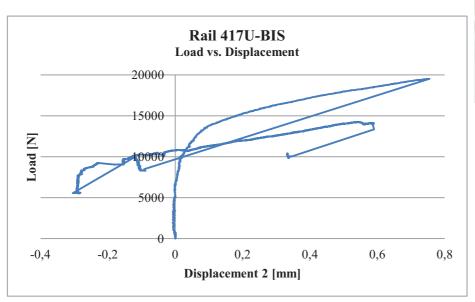




| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 16809 |
| Displacement 1 at failure [mm] | 0,02 |
| Displacement 2 at failure [mm] | 0,51 |
| Distance from crack to edge side 1 [mm] | 47 |
| Distance from crack to edge side 2 [mm] | 63 |
| Distance from crack to anchor bolt side 1 [mm] | 51 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,3 |
| Dry density [kg/m ³] | 428 |





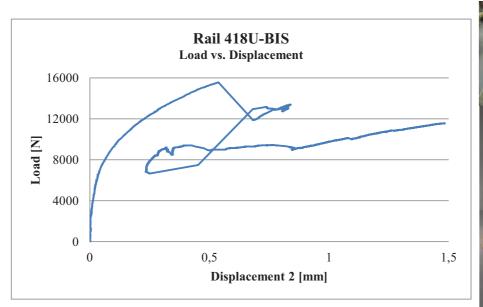




| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 19519 |
| Displacement 1 at failure [mm] | 0,08 |
| Displacement 2 at failure [mm] | 0,75 |
| Distance from crack to edge side 1 [mm] | 44 |
| Distance from crack to edge side 2 [mm] | 62 |
| Distance from crack to anchor bolt side 1 [mm] | 48 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,2 |
| Dry density [kg/m ³] | 424 |





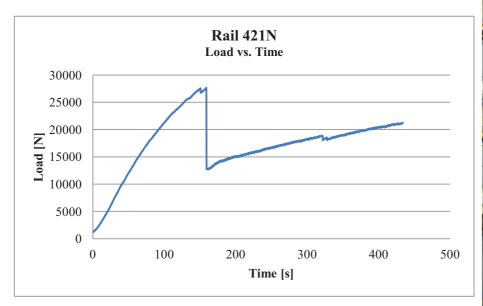




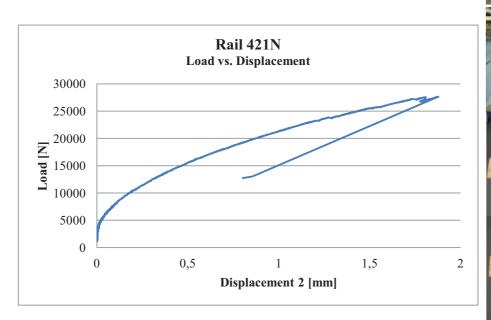
| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 15569 |
| Displacement 1 at failure [mm] | -0,02 |
| Displacement 2 at failure [mm] | 0,54 |
| Distance from crack to edge side 1 [mm] | 34 |
| Distance from crack to edge side 2 [mm] | 56 |
| Distance from crack to anchor bolt side 1 [mm] | 38 |
| Distance from crack to anchor bolt side 2 [mm] | 51 |
| Moisture [%] | 13,5 |
| Dry density [kg/m ³] | 392 |

Set 2 – Size of washer 60x60mm

Pith Down

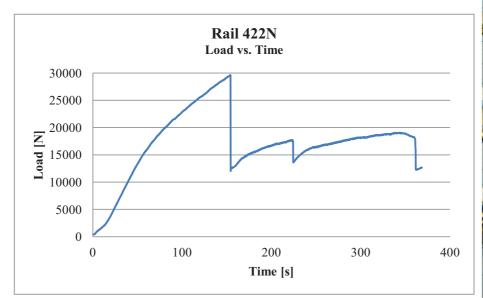




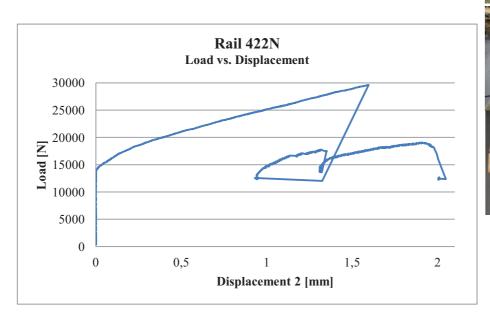




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 27643 |
| Displacement 1 at failure [mm] | 0,00 |
| Displacement 2 at failure [mm] | 1,88 |
| Distance from crack to edge side 1 [mm] | 68 |
| Distance from crack to edge side 2 [mm] | 55 |
| Distance from crack to anchor bolt side 1 [mm] | 65 |
| Distance from crack to anchor bolt side 2 [mm] | 62 |
| Moisture [%] | 13,1 |
| Dry density [kg/m ³] | 393 |

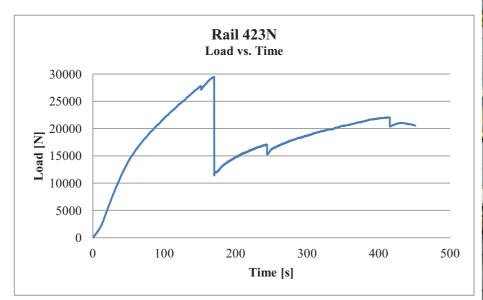




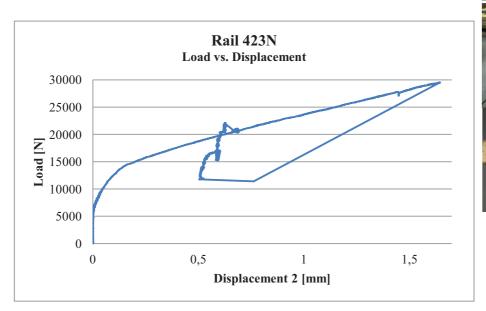




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 29616 |
| Displacement 1 at failure [mm] | 0,02 |
| Displacement 2 at failure [mm] | 1,60 |
| Distance from crack to edge side 1 [mm] | 98 |
| Distance from crack to edge side 2 [mm] | 54 |
| Distance from crack to anchor bolt side 1 [mm] | 88 |
| Distance from crack to anchor bolt side 2 [mm] | 61 |
| Moisture [%] | 13,4 |
| Dry density [kg/m ³] | 419 |

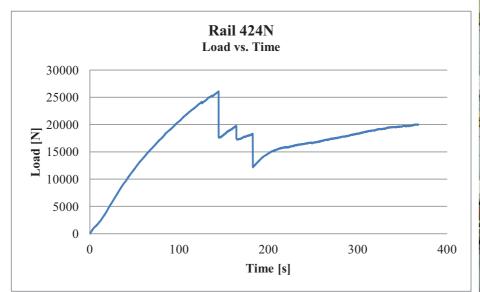




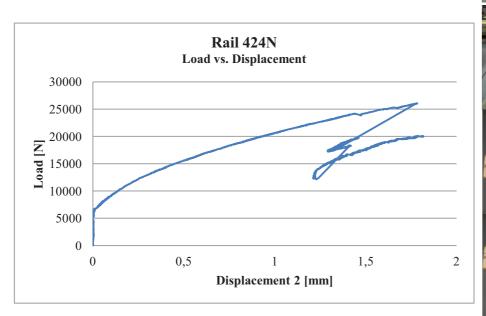




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 29506 |
| Displacement 1 at failure [mm] | -0,12 |
| Displacement 2 at failure [mm] | 1,64 |
| Distance from crack to edge side 1 [mm] | 62 |
| Distance from crack to edge side 2 [mm] | 45 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 50 |
| Moisture [%] | 13,4 |
| Dry density [kg/m ³] | 367 |

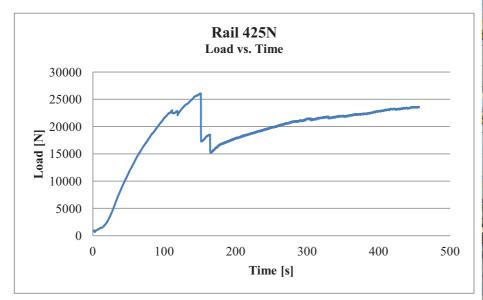




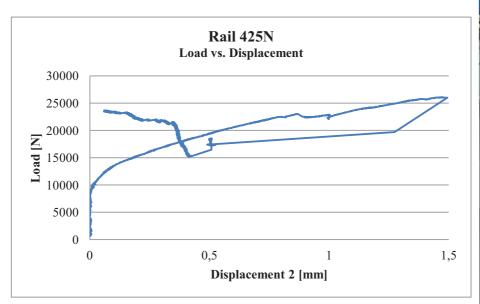




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 26065 |
| Displacement 1 at failure [mm] | 0,03 |
| Displacement 2 at failure [mm] | 1,78 |
| Distance from crack to edge side 1 [mm] | 82 |
| Distance from crack to edge side 2 [mm] | 55 |
| Distance from crack to anchor bolt side 1 [mm] | 80 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 12,3 |
| Dry density [kg/m ³] | 367 |

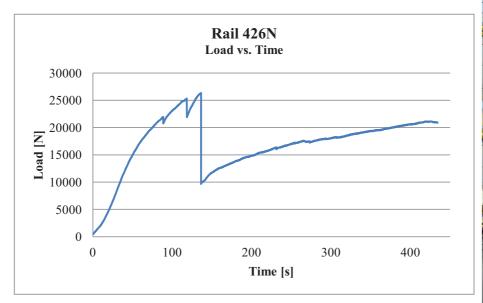




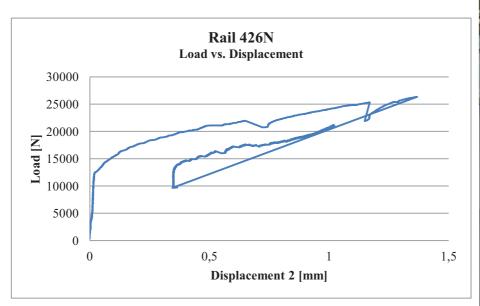




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 26069 |
| Displacement 1 at failure [mm] | -0,02 |
| Displacement 2 at failure [mm] | 1,47 |
| Distance from crack to edge side 1 [mm] | 47 |
| Distance from crack to edge side 2 [mm] | 55 |
| Distance from crack to anchor bolt side 1 [mm] | 52 |
| Distance from crack to anchor bolt side 2 [mm] | 54 |
| Moisture [%] | 13,9 |
| Dry density [kg/m ³] | 432 |

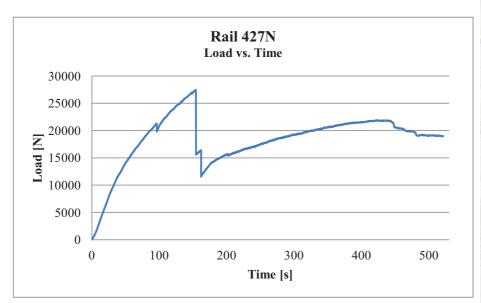




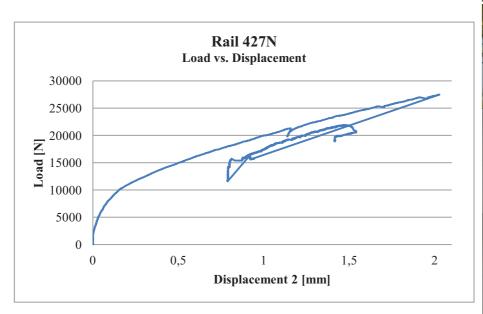




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 26334 |
| Displacement 1 at failure [mm] | 0,02 |
| Displacement 2 at failure [mm] | 1,37 |
| Distance from crack to edge side 1 [mm] | 66 |
| Distance from crack to edge side 2 [mm] | 32 |
| Distance from crack to anchor bolt side 1 [mm] | 59 |
| Distance from crack to anchor bolt side 2 [mm] | 42 |
| Moisture [%] | 12,9 |
| Dry density [kg/m ³] | 409 |

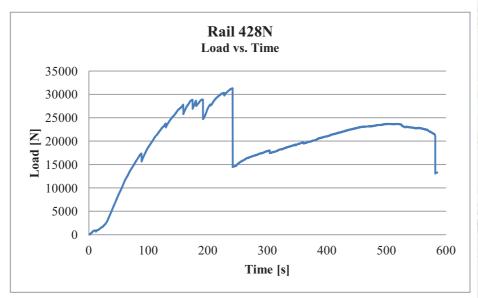




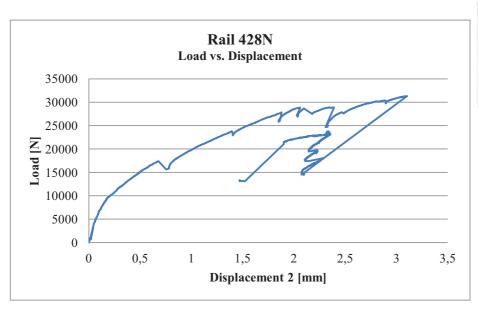




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 27485 |
| Displacement 1 at failure [mm] | 0,07 |
| Displacement 2 at failure [mm] | 2,03 |
| Distance from crack to edge side 1 [mm] | 59 |
| Distance from crack to edge side 2 [mm] | 50 |
| Distance from crack to anchor bolt side 1 [mm] | 55 |
| Distance from crack to anchor bolt side 2 [mm] | 42 |
| Moisture [%] | 12,0 |
| Dry density [kg/m ³] | 389 |



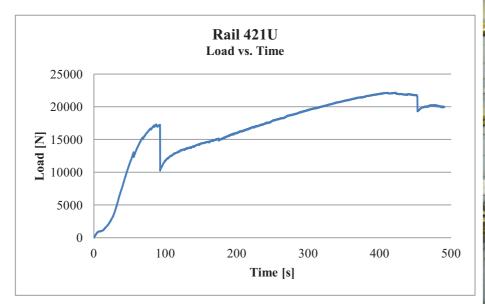




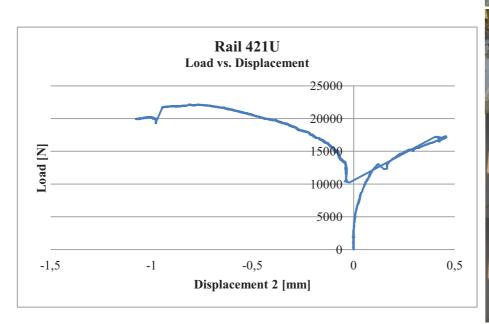


| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 31310 |
| Displacement 1 at failure [mm] | 0,05 |
| Displacement 2 at failure [mm] | 3,10 |
| Distance from crack to edge side 1 [mm] | 85 |
| Distance from crack to edge side 2 [mm] | 55 |
| Distance from crack to anchor bolt side 1 [mm] | 82 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,5 |
| Dry density [kg/m ³] | 450 |

Pith Up



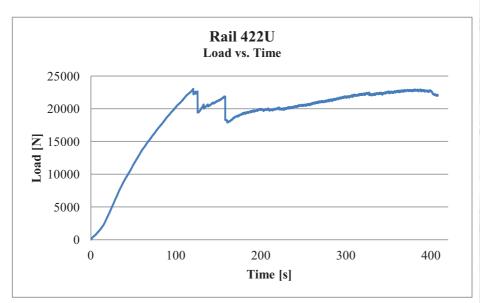




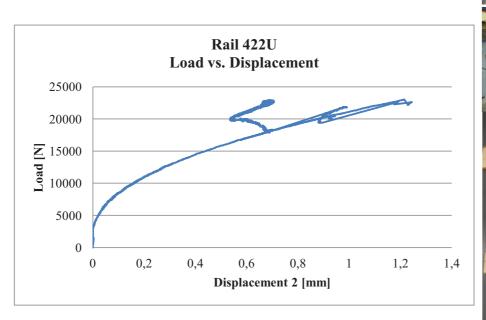


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 17315 |
| Displacement 1 at failure [mm] | -0,02 |
| Displacement 2 at failure [mm] | 0,46 |
| Distance from crack to edge side 1 [mm] | 62 |
| Distance from crack to edge side 2 [mm] | 57 |
| Distance from crack to anchor bolt side 1 [mm] | 62 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,9 |
| Dry density [kg/m ³] | 390 |

Probable problem not visible in the rail, because the failure load is under the average.

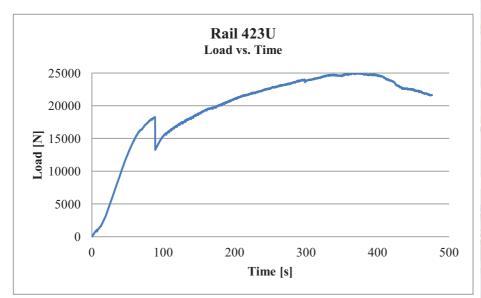




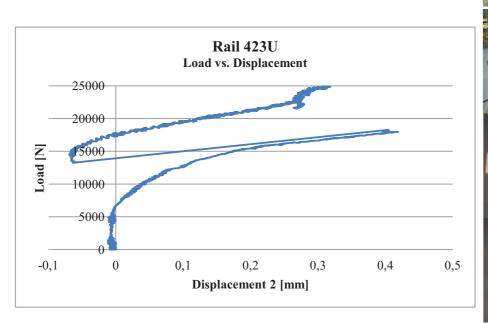




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 23037 |
| Displacement 1 at failure [mm] | 0,07 |
| Displacement 2 at failure [mm] | 1,21 |
| Distance from crack to edge side 1 [mm] | 64 |
| Distance from crack to edge side 2 [mm] | 55 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 11,0 |
| Dry density [kg/m ³] | 390 |



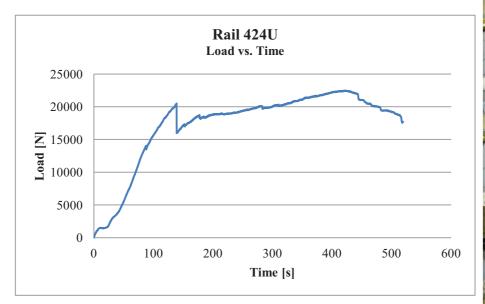




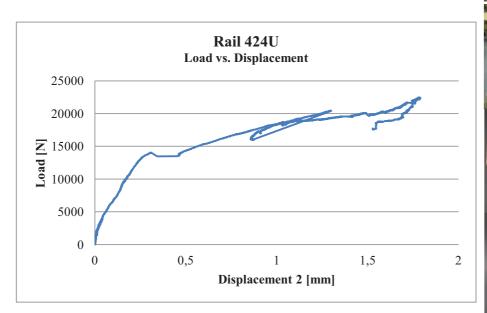


| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 18253 |
| Displacement 1 at failure [mm] | -0,02 |
| Displacement 2 at failure [mm] | 0,40 |
| Distance from crack to edge side 1 [mm] | 53 |
| Distance from crack to edge side 2 [mm] | 69 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 58 |
| Moisture [%] | 11,9 |
| Dry density [kg/m ³] | 377 |

Pre-crack on the side 2 by tightening the bolt. This had considerable influence in the test.



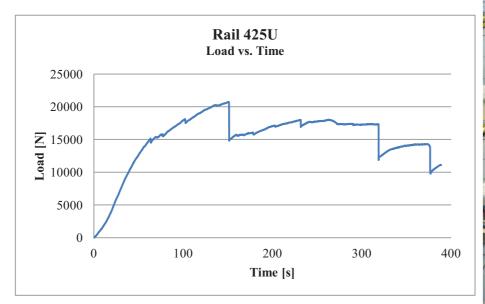




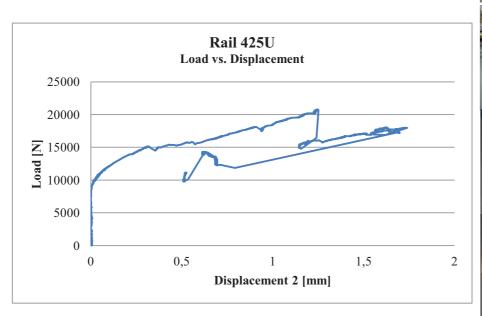


| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 20464 |
| Displacement 1 at failure [mm] | -0,01 |
| Displacement 2 at failure [mm] | 1,30 |
| Distance from crack to edge side 1 [mm] | 67 |
| Distance from crack to edge side 2 [mm] | 60 |
| Distance from crack to anchor bolt side 1 [mm] | 63 |
| Distance from crack to anchor bolt side 2 [mm] | 68 |
| Moisture [%] | 12,2 |
| Dry density [kg/m ³] | 375 |

Pre-crack on both sides.



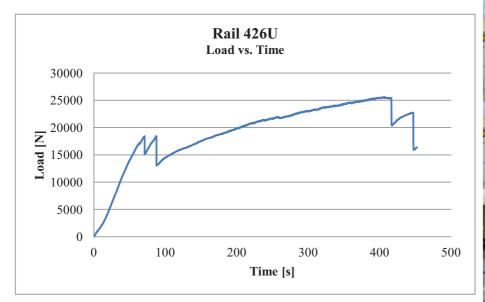




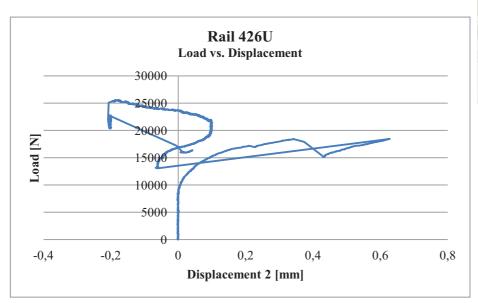


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 20768 |
| Displacement 1 at failure [mm] | -0,11 |
| Displacement 2 at failure [mm] | 1,25 |
| Distance from crack to edge side 1 [mm] | 75 |
| Distance from crack to edge side 2 [mm] | 104 |
| Distance from crack to anchor bolt side 1 [mm] | 81 |
| Distance from crack to anchor bolt side 2 [mm] | 102 |
| Moisture [%] | 12,9 |
| Dry density [kg/m ³] | 404 |

Pre-crack on the side 1. The crack started immediately from the side 1 until the side 2.



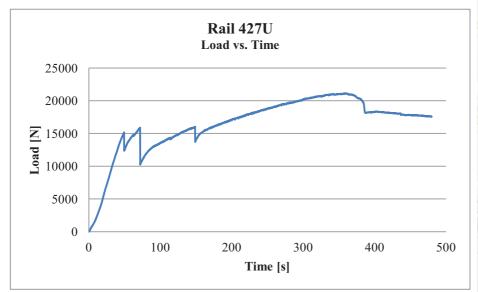




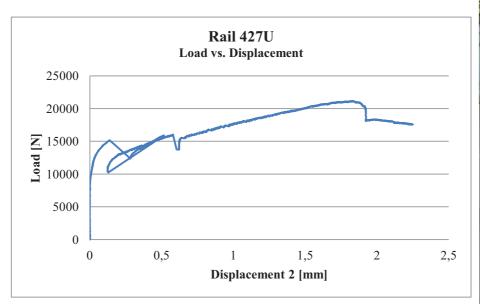


| Type of failure | Failure 1 – 1 st crack at side 1 |
|--|---|
| Failure load [N] | 18409 |
| Displacement 1 at failure [mm] | -0,01 |
| Displacement 2 at failure [mm] | 0,34 |
| Distance from crack to edge side 1 [mm] | 44 (pre-crack) – 56 (failure crack) |
| Distance from crack to edge side 2 [mm] | 62 |
| Distance from crack to anchor bolt side 1 [mm] | 48 (pre-crack) – 61 (failure crack) |
| Distance from crack to anchor bolt side 2 [mm] | 58 |
| Moisture [%] | 13,5 |
| Dry density [kg/m ³] | 437 |

First crack started from the pre-crack on the side 1 but after another crack line happened.

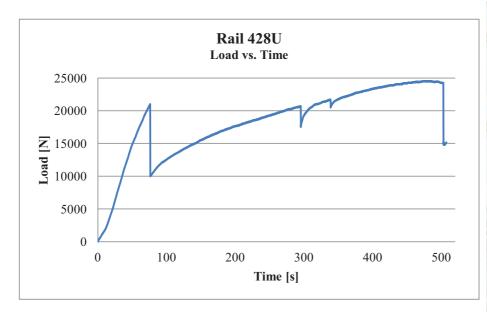




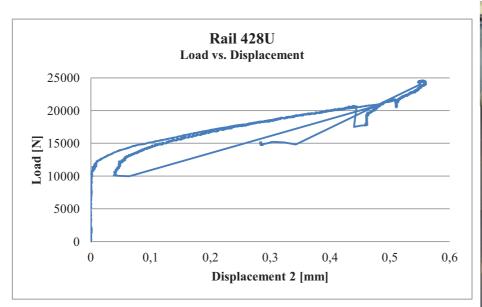




| Type of failure | Failure 1 – 1 st crack at side 1 |
|--|---|
| Failure load [N] | 15180 |
| Displacement 1 at failure [mm] | 0,00 |
| Displacement 2 at failure [mm] | 0,45 |
| Distance from crack to edge side 1 [mm] | 57 |
| Distance from crack to edge side 2 [mm] | 80 |
| Distance from crack to anchor bolt side 1 [mm] | 59 |
| Distance from crack to anchor bolt side 2 [mm] | 76 |
| Moisture [%] | 13,3 |
| Dry density [kg/m ³] | 550 |





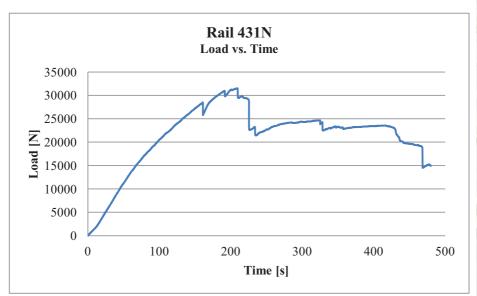




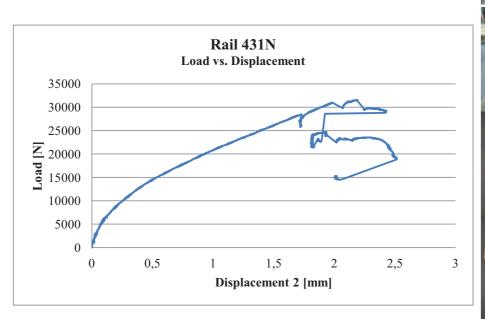
| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 21019 |
| Displacement 1 at failure [mm] | 0,02 |
| Displacement 2 at failure [mm] | 0,49 |
| Distance from crack to edge side 1 [mm] | 58 |
| Distance from crack to edge side 2 [mm] | 60 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 59 |
| Moisture [%] | 12,7 |
| Dry density [kg/m ³] | 471 |

Possible pre-crack on both sides but they seem do not have any influence on the test.

Set 3 – Size of washer 80x70 mm
Pith Down

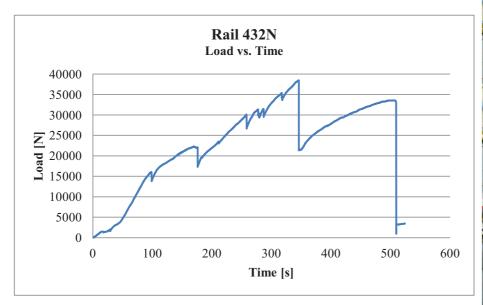




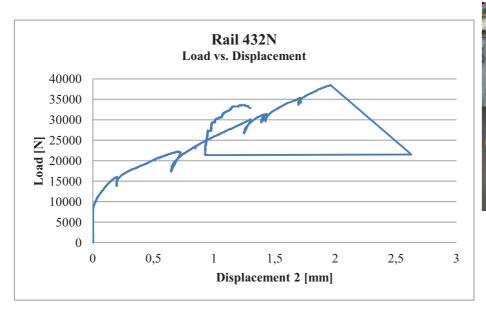




| Type of failure | Failure $2 - 1^{st}$ crack at side 1 |
|----------------------------------|--------------------------------------|
| Failure load [N] | 31530 |
| Displacement 1 at failure [mm] | 0,14 |
| Displacement 2 at failure [mm] | 2,19 |
| Moisture [%] | 14,5 |
| Dry density [kg/m ³] | 455 |



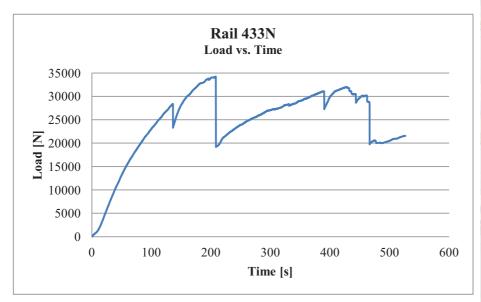




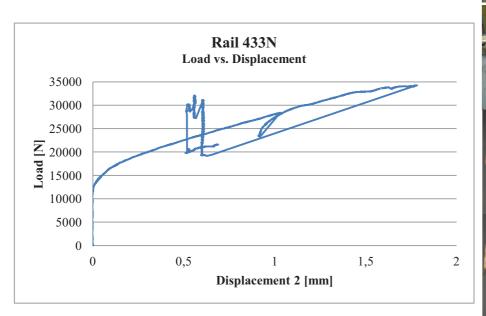


| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 38469 |
| Displacement 1 at failure [mm] | -0,01 |
| Displacement 2 at failure [mm] | 1,96 |
| Distance from crack to edge side 1 [mm] | 89 |
| Distance from crack to edge side 2 [mm] | 50 |
| Distance from crack to anchor bolt side 1 [mm] | 85 |
| Distance from crack to anchor bolt side 2 [mm] | 62 |
| Moisture [%] | 14,4 |
| Dry density [kg/m ³] | 450 |

The cracks before the failure at 38 kN are movement of the rail. Anchor bolt failure at 33 kN.

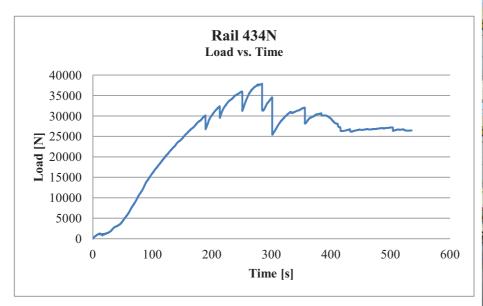




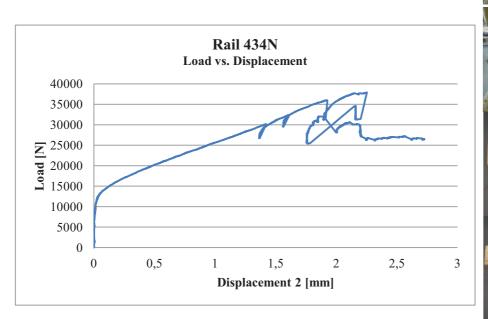




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 28381 |
| Displacement 1 at failure [mm] | 0,02 |
| Displacement 2 at failure [mm] | 1,03 |
| Distance from crack to edge side 1 [mm] | 54 |
| Distance from crack to edge side 2 [mm] | 44 |
| Distance from crack to anchor bolt side 1 [mm] | 54 |
| Distance from crack to anchor bolt side 2 [mm] | 48 |
| Moisture [%] | 12,3 |
| Dry density [kg/m ³] | 394 |



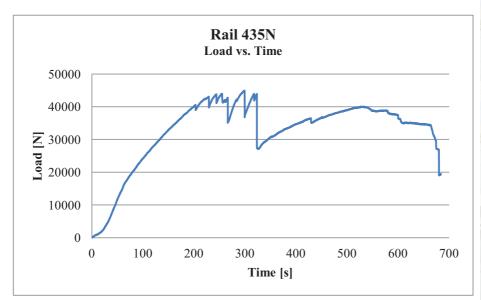




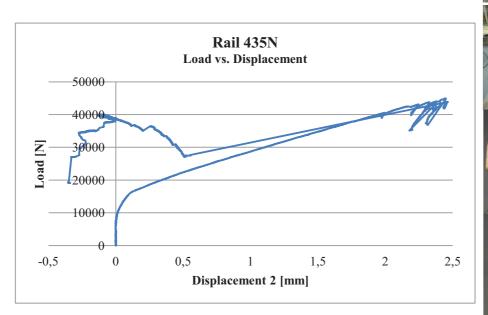


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 37884 |
| Displacement 1 at failure [mm] | 0,02 |
| Displacement 2 at failure [mm] | 2,25 |
| Distance from crack to edge side 1 [mm] | 19 |
| Distance from crack to edge side 2 [mm] | 14 |
| Distance from crack to anchor bolt side 1 [mm] | 18 |
| Distance from crack to anchor bolt side 2 [mm] | 16 |
| Moisture [%] | 12,9 |
| Dry density [kg/m ³] | 421 |

The cracks before the failure at 37 kN are movement of the rail.

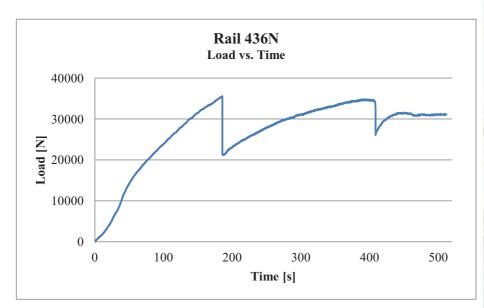




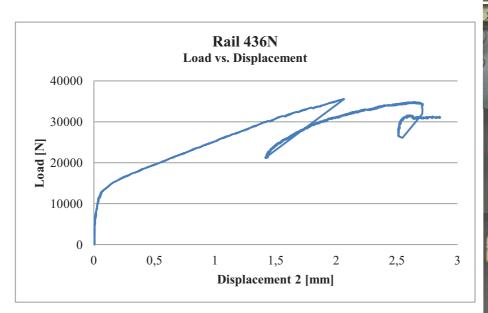




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 43987 |
| Displacement 1 at failure [mm] | 0,06 |
| Displacement 2 at failure [mm] | 2,37 |
| Distance from crack to edge side 1 [mm] | 65 |
| Distance from crack to edge side 2 [mm] | 39 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 50 |
| Moisture [%] | 11,7 |
| Dry density [kg/m ³] | 449 |

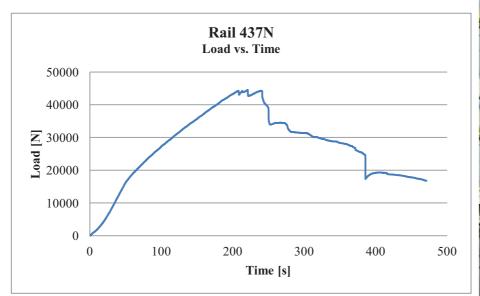




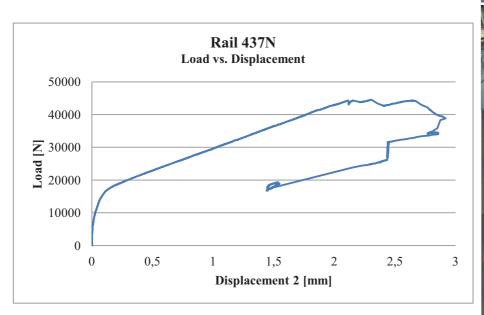




| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 35521 |
| Displacement 1 at failure [mm] | 0,03 |
| Displacement 2 at failure [mm] | 2,06 |
| Distance from crack to edge side 1 [mm] | 80 |
| Distance from crack to edge side 2 [mm] | 64 |
| Distance from crack to anchor bolt side 1 [mm] | 74 |
| Distance from crack to anchor bolt side 2 [mm] | 72 |
| Moisture [%] | 13,6 |
| Dry density [kg/m ³] | 378 |

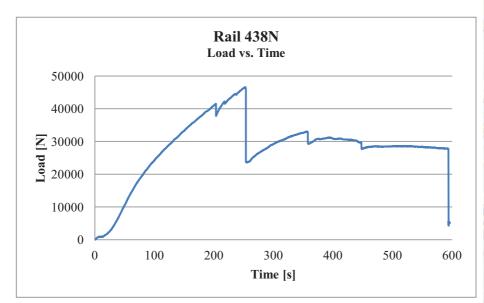




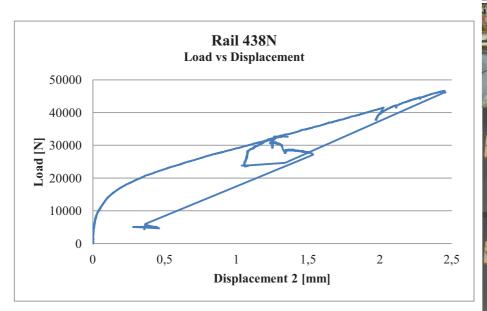




| Type of failure | Failure $2 - 1^{st}$ crack at side 1 |
|----------------------------------|--------------------------------------|
| Failure load [N] | 44512 |
| Displacement 1 at failure [mm] | 0,20 |
| Displacement 2 at failure [mm] | 2,31 |
| Moisture [%] | 14,3 |
| Dry density [kg/m ³] | 526 |



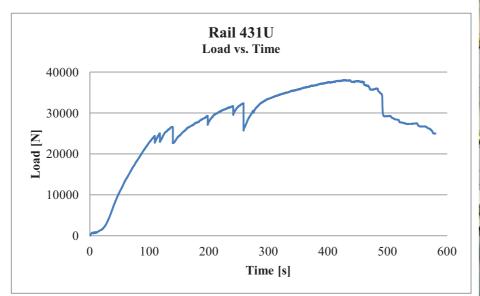




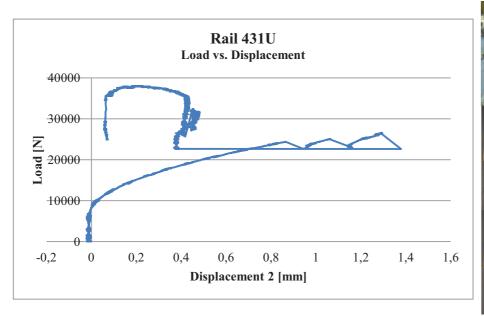


| Type of failure | Failure 1 – Instantaneous crack on both sides |
|--|---|
| Failure load [N] | 46611 |
| Displacement 1 at failure [mm] | 0,09 |
| Displacement 2 at failure [mm] | 2,45 |
| Distance from crack to edge side 1 [mm] | 91 |
| Distance from crack to edge side 2 [mm] | 69 |
| Distance from crack to anchor bolt side 1 [mm] | 88 |
| Distance from crack to anchor bolt side 2 [mm] | 77 |
| Moisture [%] | 11,4 |
| Dry density [kg/m ³] | 454 |

Pith Up

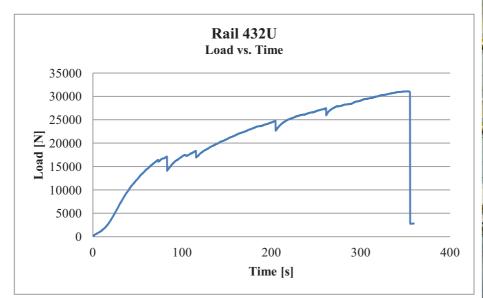




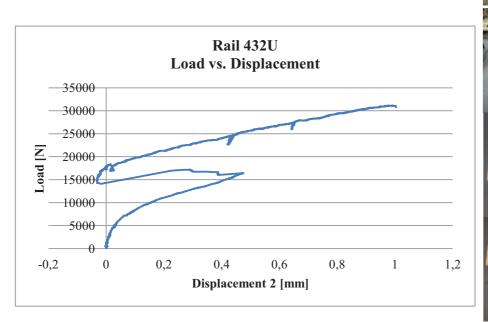




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 26576 |
| Displacement 1 at failure [mm] | 0,04 |
| Displacement 2 at failure [mm] | 1,29 |
| Distance from crack to edge side 1 [mm] | 56 |
| Distance from crack to edge side 2 [mm] | 63 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 14,6 |
| Dry density [kg/m ³] | 464 |



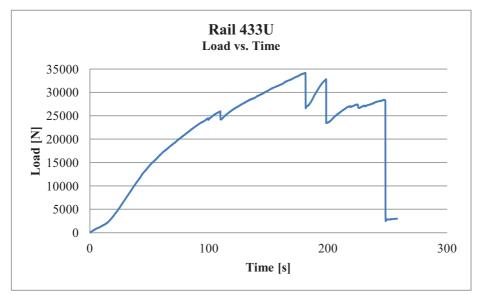




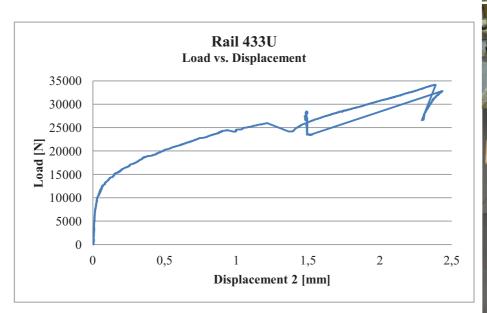


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 17161 |
| Displacement 1 at failure [mm] | -0,04 |
| Displacement 2 at failure [mm] | 0,28 |
| Distance from crack to edge side 1 [mm] | 55 |
| Distance from crack to edge side 2 [mm] | 86 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 81 |
| Moisture [%] | 11,8 |
| Dry density [kg/m ³] | 394 |

Pre-crack on the side 1 by tightening the bolt. This had considerable influence in the test.



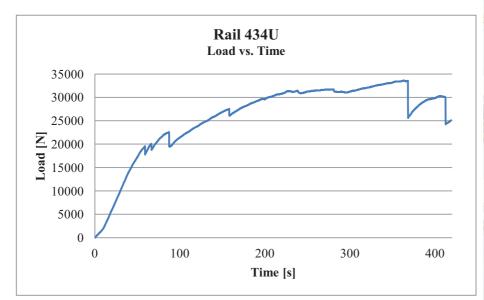




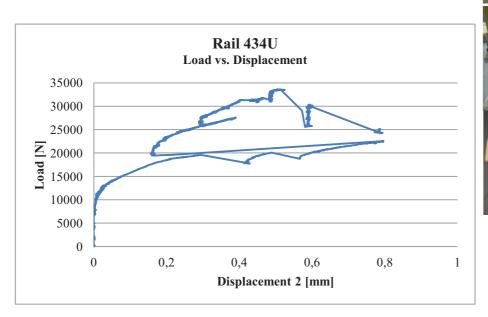


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 34145 |
| Displacement 1 at failure [mm] | 0,06 |
| Displacement 2 at failure [mm] | 2,38 |
| Distance from crack to edge side 1 [mm] | 29 |
| Distance from crack to edge side 2 [mm] | 59 |
| Distance from crack to anchor bolt side 1 [mm] | 30 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 14,0 |
| Dry density [kg/m ³] | 489 |

The last crack is caused by the anchor bolt failure on the side 2.

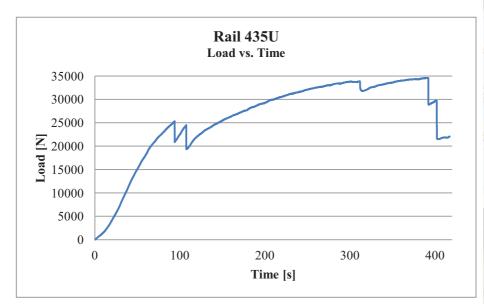




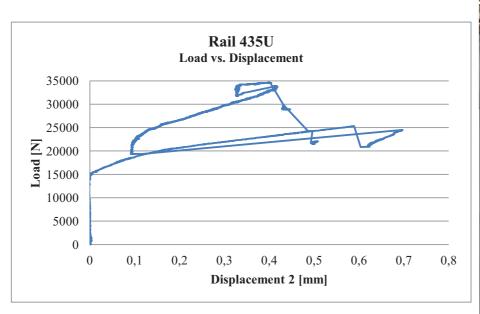




| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 22564 |
| Displacement 1 at failure [mm] | 0,01 |
| Displacement 2 at failure [mm] | 0,80 |
| Distance from crack to edge side 1 [mm] | 54 |
| Distance from crack to edge side 2 [mm] | 75 |
| Distance from crack to anchor bolt side 1 [mm] | 59 |
| Distance from crack to anchor bolt side 2 [mm] | 71 |
| Moisture [%] | 13,1 |
| Dry density [kg/m ³] | 425 |

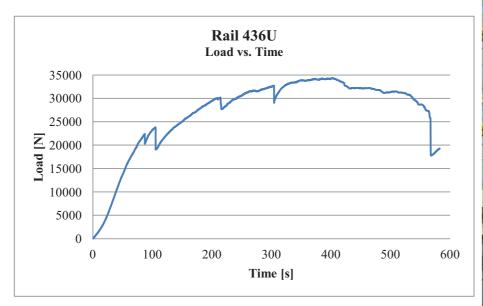




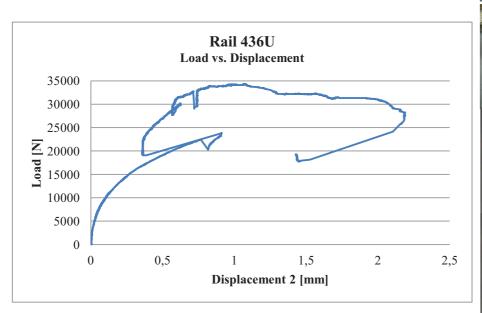




| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 24986 |
| Displacement 1 at failure [mm] | 0,03 |
| Displacement 2 at failure [mm] | 0,56 |
| Distance from crack to edge side 1 [mm] | 57 |
| Distance from crack to edge side 2 [mm] | 75 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 72 |
| Moisture [%] | 13,2 |
| Dry density [kg/m ³] | 411 |



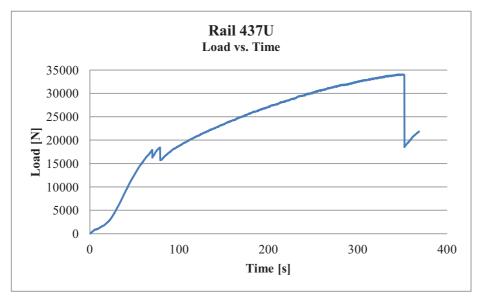




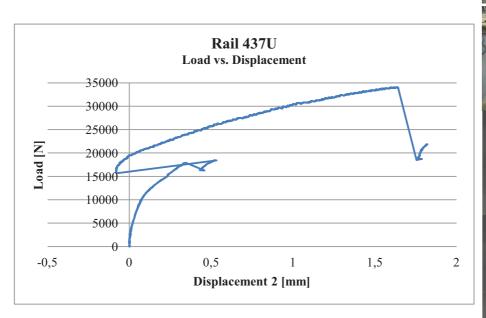


| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 23822 |
| Displacement 1 at failure [mm] | 0,05 |
| Displacement 2 at failure [mm] | 0,91 |
| Distance from crack to edge side 1 [mm] | 58 |
| Distance from crack to edge side 2 [mm] | 80 |
| Distance from crack to anchor bolt side 1 [mm] | 59 |
| Distance from crack to anchor bolt side 2 [mm] | 76 |
| Moisture [%] | - |
| Dry density [kg/m ³] | - |

Due problems with the rail, moisture and density were not measured.



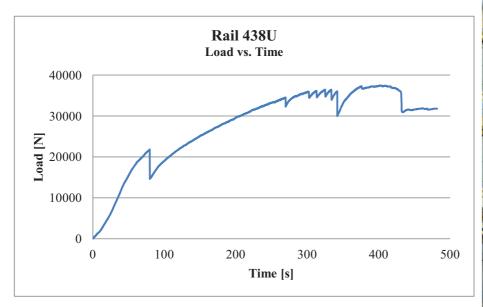




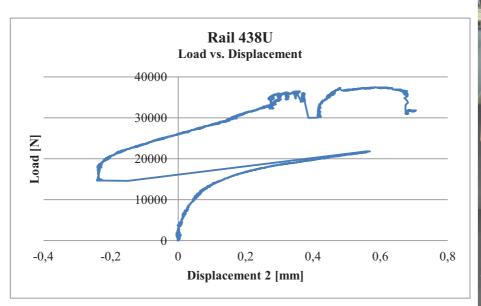


| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 18467 |
| Displacement 1 at failure [mm] | 0,00 |
| Displacement 2 at failure [mm] | 0,52 |
| Distance from crack to edge side 1 [mm] | 60 |
| Distance from crack to edge side 2 [mm] | 60 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,2 |
| Dry density [kg/m ³] | 371 |

Pre-crack on the side 2 by tightening the bolt. This had considerable influence in the test.







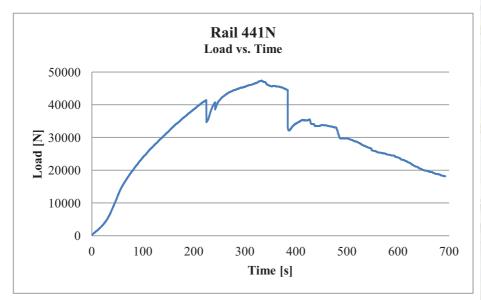


| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 21747 |
| Displacement 1 at failure [mm] | 0,03 |
| Displacement 2 at failure [mm] | 0,56 |
| Distance from crack to edge side 1 [mm] | 54 |
| Distance from crack to edge side 2 [mm] | 52 |
| Distance from crack to anchor bolt side 1 [mm] | 62 |
| Distance from crack to anchor bolt side 2 [mm] | 57 |
| Moisture [%] | 11,5 |
| Dry density [kg/m ³] | 433 |

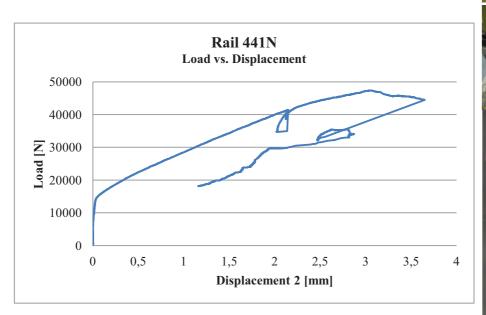
Pre-crack on the side 2 by tightening the bolt. This had considerable influence in the test.

Set 4 – Size of washer 100x70 mm

Pith down

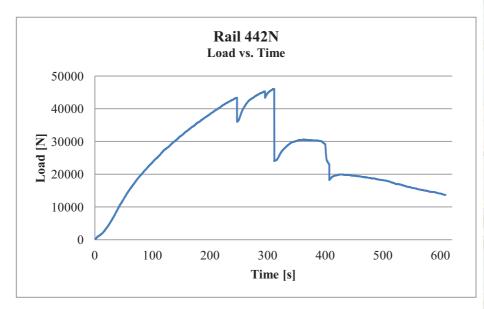




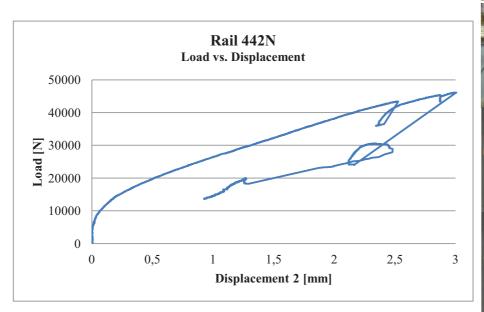




| Type of failure | Failure $2 - 1^{st}$ crack at side 2 |
|----------------------------------|--------------------------------------|
| Failure load [N] | 47372 |
| Displacement 1 at failure [mm] | 0,16 |
| Displacement 2 at failure [mm] | 3,06 |
| Moisture [%] | 12,9 |
| Dry density [kg/m ³] | 395 |

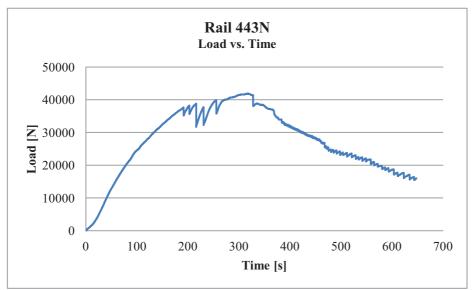




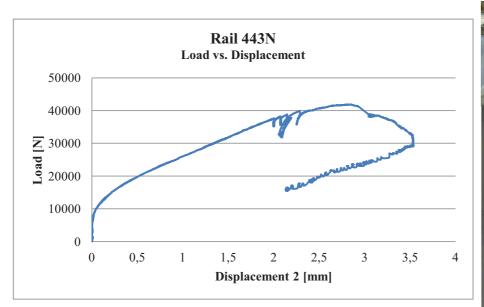




| Type of failure | Failure $2 - 1^{st}$ crack at side 1 |
|----------------------------------|--------------------------------------|
| Failure load [N] | 46087 |
| Displacement 1 at failure [mm] | 0,10 |
| Displacement 2 at failure [mm] | 2,99 |
| Moisture [%] | 12,0 |
| Dry density [kg/m ³] | 433 |

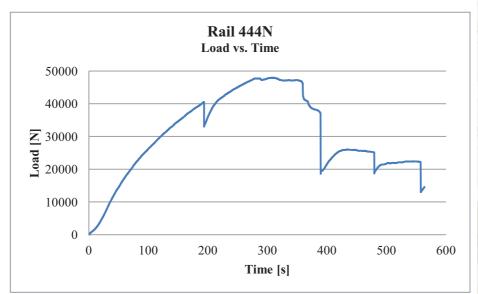




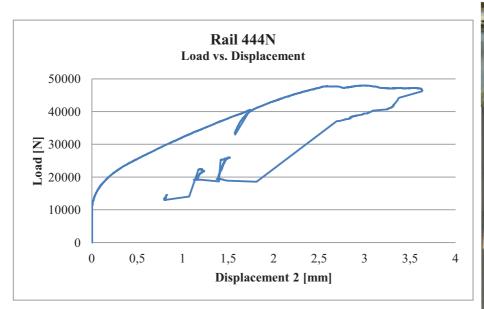




| Type of failure | Failure 3 |
|----------------------------------|-----------|
| Failure load [N] | 41868 |
| Displacement 1 at failure [mm] | 0,07 |
| Displacement 2 at failure [mm] | 2,80 |
| Moisture [%] | 11,6 |
| Dry density [kg/m ³] | 385 |

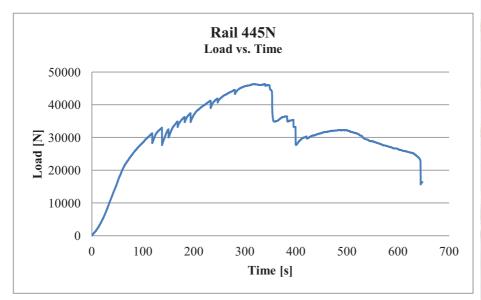




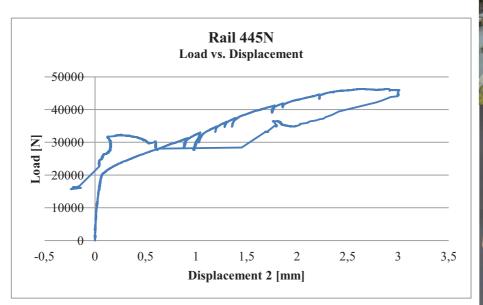




| Type of failure | Failure $2 - 1^{st}$ crack at side 1 |
|----------------------------------|--------------------------------------|
| Failure load [N] | 47952 |
| Displacement 1 at failure [mm] | 0,18 |
| Displacement 2 at failure [mm] | 2,99 |
| Moisture [%] | 13,5 |
| Dry density [kg/m ³] | 410 |



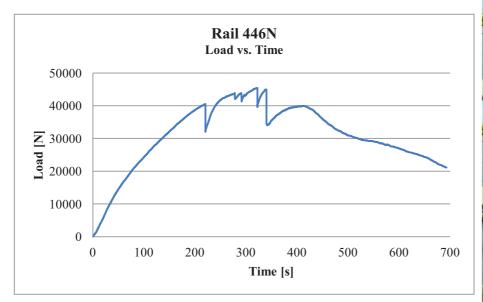




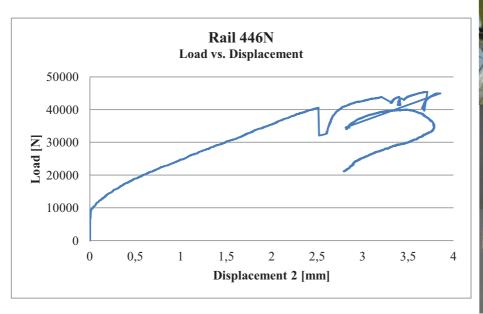
| The state of the s | |
|--|--|
| 445N | |
| NORSA-S = W020 0407 CE | |
| | |
| NORRA-S = W020 0407 24 | |
| 19.10 | |

| Type of failure | Failure 3 |
|----------------------------------|-----------|
| Failure load [N] | 46306 |
| Displacement 1 at failure [mm] | 0,15 |
| Displacement 2 at failure [mm] | 2,90 |
| Moisture [%] | 12,8 |
| Dry density [kg/m ³] | 400 |

The bottom rail failure happens after the nails pull-out.

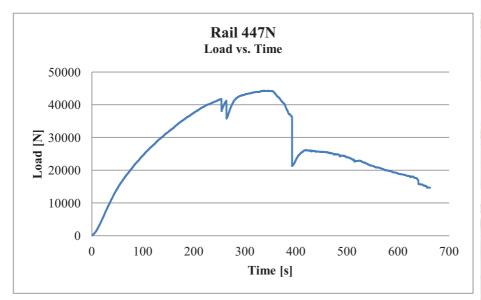




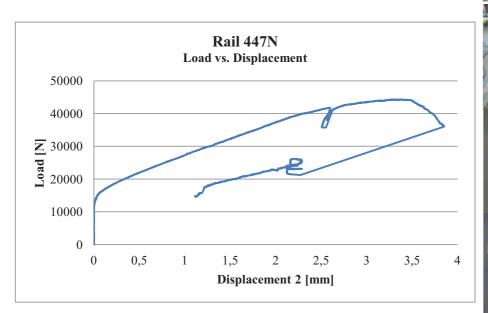




| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 45414 |
| Displacement 1 at failure [mm] | 0,26 |
| Displacement 2 at failure [mm] | 3,71 |
| Distance from crack to edge side 1 [mm] | 50 |
| Distance from crack to edge side 2 [mm] | 24 |
| Distance from crack to anchor bolt side 1 [mm] | 54 |
| Distance from crack to anchor bolt side 2 [mm] | 17 |
| Moisture [%] | 12,7 |
| Dry density [kg/m ³] | 396 |



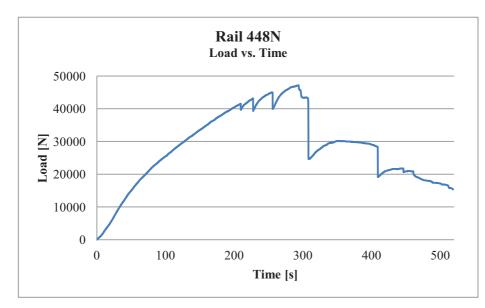




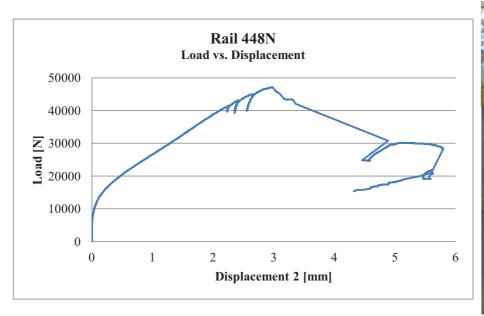
| 3 |
|-----------------------------|
| Value 2 |
| 447N |
| |
| שלון. אבע + נגל לי במפנה לי |
| |
| 167.5 |
| 16.14 CON ENERGY |
| |
| |

| Type of failure | Failure 3 |
|----------------------------------|-----------|
| Failure load [N] | 44278 |
| Displacement 1 at failure [mm] | 0,12 |
| Displacement 2 at failure [mm] | 3,38 |
| Moisture [%] | 10,0 |
| Dry density [kg/m ³] | 390 |

After test some crack was found on the rail in the nails line. However the first type of failure is nails pull-out.



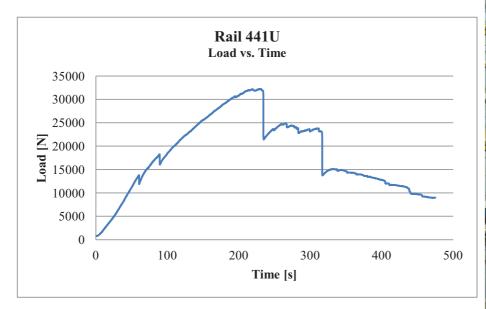




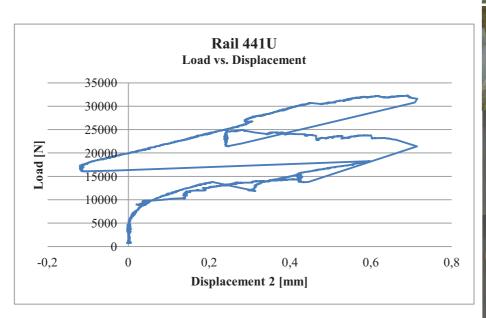


| Type of failure | Failure $2 - 1^{st}$ crack at side 2 |
|----------------------------------|--------------------------------------|
| Failure load [N] | 47164 |
| Displacement 1 at failure [mm] | 0,16 |
| Displacement 2 at failure [mm] | 2,97 |
| Moisture [%] | 12,3 |
| Dry density [kg/m ³] | 380 |

Pith Up



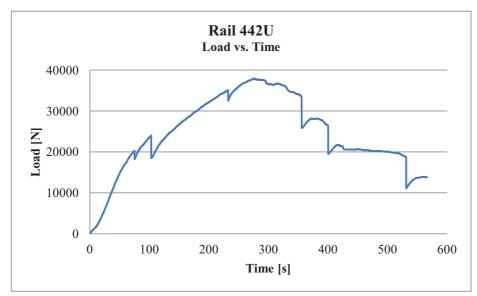




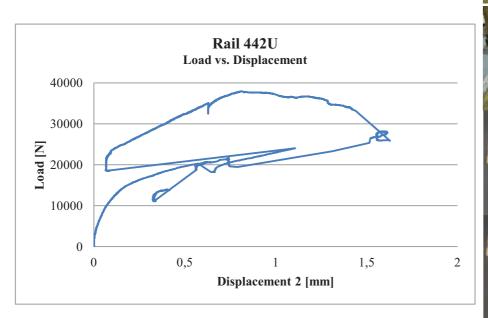


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 13807 |
| Displacement 1 at failure [mm] | 0,02 |
| Displacement 2 at failure [mm] | 0,21 |
| Distance from crack to edge side 1 [mm] | 57 |
| Distance from crack to edge side 2 [mm] | 60 |
| Distance from crack to anchor bolt side 1 [mm] | 57 |
| Distance from crack to anchor bolt side 2 [mm] | 59 |
| Moisture [%] | 10,8 |
| Dry density [kg/m ³] | 370 |

Pre-crack on the side 1, without it the failure would have been crack in the nails line.



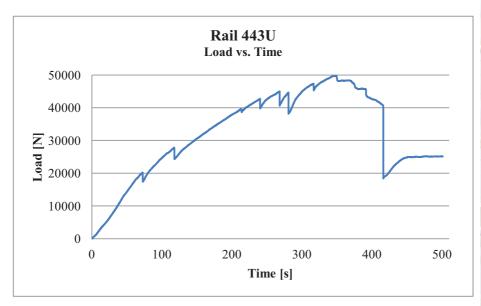




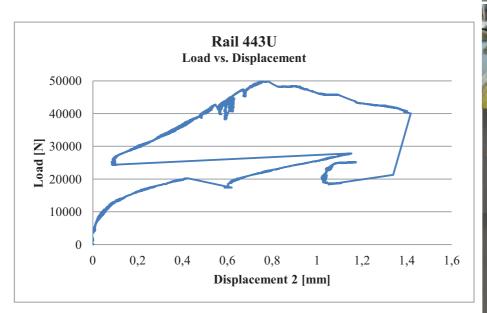


| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 24015 |
| Displacement 1 at failure [mm] | 0,08 |
| Displacement 2 at failure [mm] | 1,11 |
| Distance from crack to edge side 1 [mm] | 57 |
| Distance from crack to edge side 2 [mm] | 59 |
| Distance from crack to anchor bolt side 1 [mm] | 57 |
| Distance from crack to anchor bolt side 2 [mm] | 59 |
| Moisture [%] | 14,2 |
| Dry density [kg/m ³] | 469 |

After the crack at 24 kN the load increase a lot until 38 kN. Probably the failure type is 2.



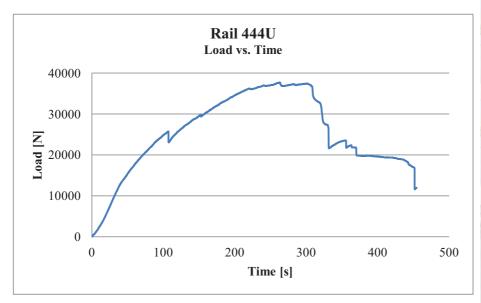




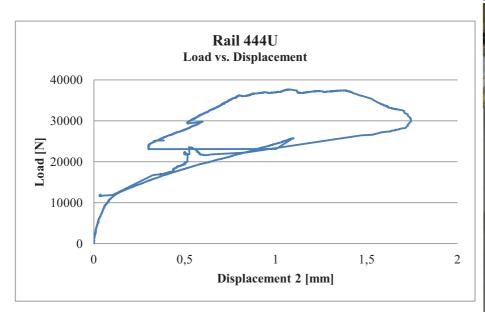


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 20250 |
| Displacement 1 at failure [mm] | 0,02 |
| Displacement 2 at failure [mm] | 0,42 |
| Distance from crack to edge side 1 [mm] | 52 |
| Distance from crack to edge side 2 [mm] | 63 |
| Distance from crack to anchor bolt side 1 [mm] | 62 |
| Distance from crack to anchor bolt side 2 [mm] | 63 |
| Moisture [%] | 12,0 |
| Dry density [kg/m ³] | 451 |

Failure 1 caused by pre-crack on side 1 but the failure type could be 2.



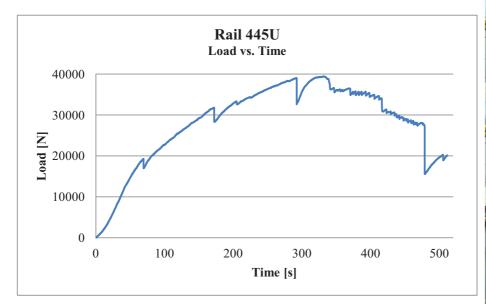




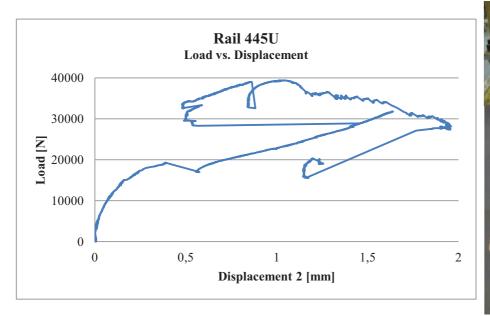


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 25737 |
| Displacement 1 at failure [mm] | 0,13 |
| Displacement 2 at failure [mm] | 1,08 |
| Distance from crack to edge side 1 [mm] | 47 |
| Distance from crack to edge side 2 [mm] | 60 |
| Distance from crack to anchor bolt side 1 [mm] | 62 |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 11,3 |
| Dry density [kg/m ³] | 398 |

Failure 1 caused by pre-crack on side 1 but the failure type could be 2.



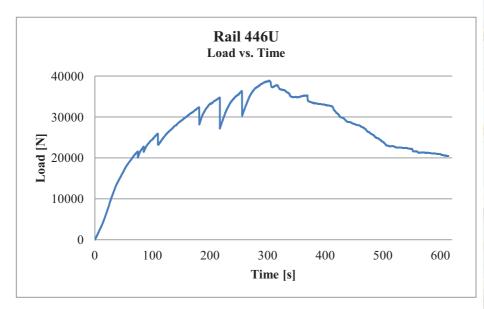




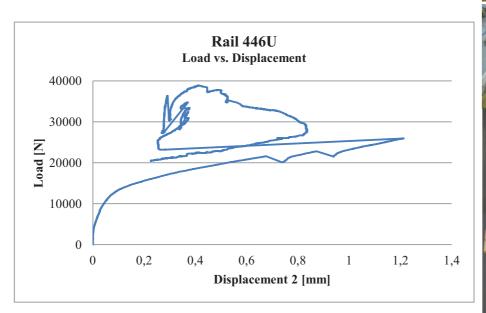


| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 19253 |
| Displacement 1 at failure [mm] | 0,00 |
| Displacement 2 at failure [mm] | 0,39 |
| Distance from crack to edge side 1 [mm] | 65 (pre-crack) – 46 (crack line) |
| Distance from crack to edge side 2 [mm] | 68 |
| Distance from crack to anchor bolt side 1 [mm] | 70 (pre-crack) – 41 (crack line) |
| Distance from crack to anchor bolt side 2 [mm] | 60 |
| Moisture [%] | 13,1 |
| Dry density [kg/m ³] | 421 |

Pre-crack on side 2 tightening the anchor bolt, without it failure type would have been 2.



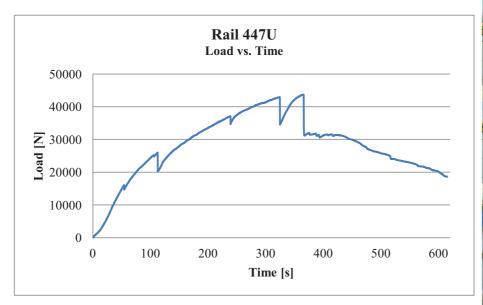




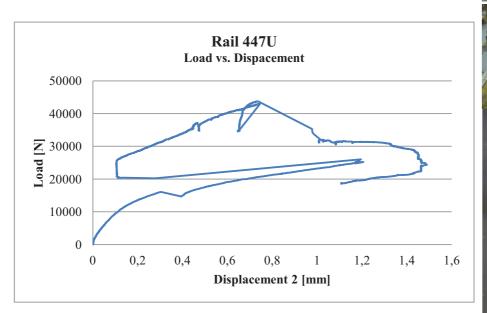


| Type of failure | Failure $1 - 1^{st}$ crack at side 2 |
|--|--------------------------------------|
| Failure load [N] | 25930 |
| Displacement 1 at failure [mm] | 0,04 |
| Displacement 2 at failure [mm] | 1,21 |
| Distance from crack to edge side 1 [mm] | 57 |
| Distance from crack to edge side 2 [mm] | 60 |
| Distance from crack to anchor bolt side 1 [mm] | 59 |
| Distance from crack to anchor bolt side 2 [mm] | 59 |
| Moisture [%] | 13,1 |
| Dry density [kg/m ³] | 490 |

After the crack at 26 kN the load increase a lot until 39 kN causing the failure type 2 and 3.



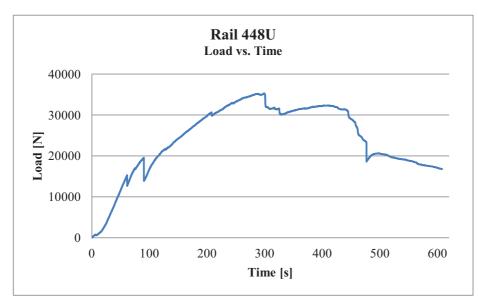




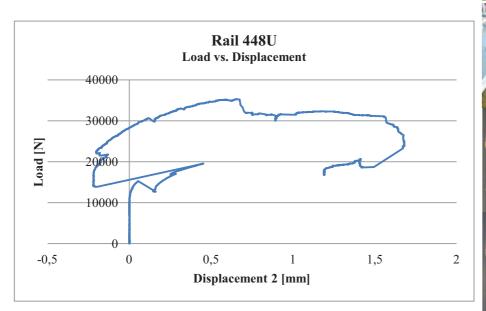


| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 16068 |
| Displacement 1 at failure [mm] | 0,04 |
| Displacement 2 at failure [mm] | 0,30 |
| Distance from crack to edge side 1 [mm] | 63 |
| Distance from crack to edge side 2 [mm] | 55 |
| Distance from crack to anchor bolt side 1 [mm] | 60 |
| Distance from crack to anchor bolt side 2 [mm] | 59 |
| Moisture [%] | 11,2 |
| Dry density [kg/m ³] | 385 |

After the crack at 16 kN the load increase a lot until 44 kN causing the failure type 2.









| Type of failure | Failure $1 - 1^{st}$ crack at side 1 |
|--|--------------------------------------|
| Failure load [N] | 15266 |
| Displacement 1 at failure [mm] | -0,03 |
| Displacement 2 at failure [mm] | 0,05 |
| Distance from crack to edge side 1 [mm] | 18 |
| Distance from crack to edge side 2 [mm] | 66 |
| Distance from crack to anchor bolt side 1 [mm] | 30 |
| Distance from crack to anchor bolt side 2 [mm] | 61 |
| Moisture [%] | 9,97 |
| Dry density [kg/m ³] | 398 |

After the crack at 15 kN the load increase a lot until 35 kN causing the failure type 2.

$\label{eq:Appendix B-Chronological summary of the conduction of the tests.}$

| | Construction | Testing | Dens. & | | Failure |
|----------|--------------|------------|------------|---|---------|
| Specimen | date | date | Moist. C. | Comments | mode |
| | | | Date | | |
| 411U | 07/06/2011 | 08/06/2011 | 10/06/2011 | - | 1 |
| 411N | 07/06/2011 | 08/06/2011 | 10/06/2011 | - | 1 |
| 412U | 07/06/2011 | 09/06/2011 | 10/06/2011 | Close to the hole for the anchor bolt in the rail on side 1 by mistake there was another hole. However this had no influence on the test. | 1 |
| 412N | 07/06/2011 | 09/06/2011 | 10/06/2011 | - | 1 |
| 413U | 07/06/2011 | 09/06/2011 | 10/06/2011 | Probably there was some problem not visible in the rail because the failure load is well below the average. | 1 |
| 413N | 07/06/2011 | 09/06/2011 | 10/06/2011 | - | 1 |
| 414U | 07/06/2011 | 09/06/2011 | 10/06/2011 | - | 1 |
| 414N | 07/06/2011 | 09/06/2011 | 10/06/2011 | - | 1 |
| 415U | 07/06/2011 | 09/06/2011 | 10/06/2011 | Influence of the pre-crack present on the side 2. | 1 |
| 415N | 07/06/2011 | 09/06/2011 | 10/06/2011 | - | 1 |
| 416U | 07/06/2011 | 09/06/2011 | 10/06/2011 | - | 1 |
| 416N | 07/06/2011 | 09/06/2011 | 10/06/2011 | - | 1 |
| 417U | 07/06/2011 | 09/06/2011 | 10/06/2011 | - | 1 |
| 417N | 07/06/2011 | 09/06/2011 | 10/06/2011 | Close to the hole for the anchor bolt in the rail on side 2 by mistake there was another hole. However this had no influence on the test. | 1 |
| 418U | 07/06/2011 | 10/06/2011 | 10/06/2011 | - | 1 |
| 418N | 07/06/2011 | 10/06/2011 | 10/06/2011 | - | 1 |
| 411U-BIS | 23/06/2011 | 23/06/2011 | 23/06/2011 | - | 1 |
| 411N-BIS | 23/06/2011 | 23/06/2011 | 23/06/2011 | - | 1 |
| 412U-BIS | 23/06/2011 | 23/06/2011 | 23/06/2011 | - | 1 |
| 412N-BIS | 23/06/2011 | 23/06/2011 | 23/06/2011 | - | 1 |
| 413U-BIS | 23/06/2011 | 23/06/2011 | 23/06/2011 | - | 1 |
| 413N-BIS | 23/06/2011 | 23/06/2011 | 23/06/2011 | - | 1 |
| 414U-BIS | 23/06/2011 | 24/06/2011 | 24/06/2011 | - | 1 |
| 414N-BIS | 23/06/2011 | 24/06/2011 | 24/06/2011 | - | 1 |
| 415U-BIS | 23/06/2011 | 24/06/2011 | 24/06/2011 | - | 1 |
| 415N-BIS | 23/06/2011 | 24/06/2011 | 24/06/2011 | - | 1 |
| 416U-BIS | 24/06/2011 | 24/06/2011 | 24/06/2011 | - | 1 |

| 416N-BIS | 24/06/2011 | 24/06/2011 | 24/06/2011 | - | 1 |
|----------|-------------|------------|------------|---------------------------------|---|
| 417U-BIS | 24/06/2011 | 24/06/2011 | 24/06/2011 | - | 1 |
| 417N-BIS | 24/06/2011 | 24/06/2011 | 24/06/2011 | Close to the hole for the | 1 |
| | | | | anchor bolt in the rail on side | |
| | | | | 2 by mistake there was | |
| | | | | another hole. However this | |
| | | | | had no influence on the test. | |
| 418U-BIS | 24/06/2011 | 24/06/2011 | 24/06/2011 | - | 1 |
| 418N-BIS | 24/06/2011 | 24/06/2011 | 24/06/2011 | - | 1 |
| 421U | 10/06/2011 | 13/06/2011 | 13/06/2011 | Probably there was some | 1 |
| | | | | problem not visible in the | |
| | | | | rail because the failure load | |
| | | | | is well below the average. | |
| 421N | 10/06/2011 | 13/06/2011 | 13/06/2011 | - | 1 |
| 422U | 10/06/2011 | 13/06/2011 | 13/06/2011 | _ | 1 |
| 422N | 10/06/2011 | 13/06/2011 | 13/06/2011 | _ | 1 |
| 423U | 10/06/2011 | 13/06/2011 | 13/06/2011 | Pre-crack on the side 2 by | 1 |
| 1230 | 10/00/2011 | 13/00/2011 | 13/00/2011 | tightening the bolt. | 1 |
| 423N | 10/06/2011 | 13/06/2011 | 13/06/2011 | tightening the boit. | 1 |
| 424U | 10/06/2011 | 13/06/2011 | 13/06/2011 | Pre-crack on both sides of | 1 |
| 4240 | 10/00/2011 | 13/00/2011 | 13/00/2011 | the rail. | 1 |
| 424N | 10/06/2011 | 13/06/2011 | 13/06/2011 | - | 1 |
| 425U | 13/06/2011 | 14/06/2011 | 14/06/2011 | Pre-crack on the side 1 of the | 1 |
| | | | | rail. | |
| 425N | 13/06/2011 | 14/06/2011 | 14/06/2011 | - | 1 |
| 426U | 13/06/2011 | 14/06/2011 | 14/06/2011 | Pre-crack on the side 1 of the | 1 |
| | | | | rail. First crack started from | |
| | | | | the pre-crack but after | |
| | | | | another crack line happened. | |
| 426N | 13/06/2011 | 14/06/2011 | 14/06/2011 | - | 1 |
| 427U | 13/06/2011 | 14/06/2011 | 14/06/2011 | - | 1 |
| 427N | 13/06/2011 | 14/06/2011 | 14/06/2011 | - | 1 |
| 428U | 13/06/2011 | 14/06/2011 | 14/06/2011 | Possible pre-crack on both | 1 |
| | | | | sides but they seem do not | |
| | | | | have any influence on the | |
| | | | | test. | |
| 428N | 13/06/2011 | 14/06/2011 | 14/06/2011 | - | 1 |
| 431U | 14/06/2011 | 15/06/2011 | 15/06/2011 | _ | 1 |
| 431N | 14/06/2011 | 15/06/2011 | 15/06/2011 | _ | 2 |
| 432U | 14/06/2011 | 15/06/2011 | 15/06/2011 | Pre-crack on the side 1 by | 1 |
| | 1.,00,2011 | | 10,00,2011 | tightening the bolt. | - |
| 432N | 14/06/2011 | 15/06/2011 | 15/06/2011 | - | 1 |
| 433U | 14/06/2011 | 15/06/2011 | 15/06/2011 | Anchor bolt failure during | 1 |
| .550 | 1,,00,2011 | 10,00,2011 | 10,00,2011 | the test on the side 2. | • |
| 433N | 14/06/2011 | 15/06/2011 | 15/06/2011 | - | 1 |
| 15511 | 1 1/00/2011 | 13/00/2011 | 13/00/2011 | | 1 |

| 434U 14/06/2011 15/06/2011 15/06/2011 - 1 434N 14/06/2011 15/06/2011 15/06/2011 - 1 435U 15/06/2011 16/06/2011 16/06/2011 - 1 435N 15/06/2011 16/06/2011 16/06/2011 - 1 436U 15/06/2011 16/06/2011 16/06/2011 Moisture and density are not measured. 436N 15/06/2011 16/06/2011 16/06/2011 - 1 437U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by tightening the bolt. 437N 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by tightening the bolt. |
|---|
| 435U 15/06/2011 16/06/2011 16/06/2011 - 1 435N 15/06/2011 16/06/2011 16/06/2011 - 1 436U 15/06/2011 16/06/2011 16/06/2011 Moisture and density are not measured. 1 436N 15/06/2011 16/06/2011 16/06/2011 - 1 437U 15/06/2011 16/06/2011 Pre-crack on the side 2 by tightening the bolt. 1 437N 15/06/2011 16/06/2011 16/06/2011 - 2 438U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by 1 |
| 435N 15/06/2011 16/06/2011 16/06/2011 - 1 436U 15/06/2011 16/06/2011 16/06/2011 Moisture and density are not measured. 1 436N 15/06/2011 16/06/2011 16/06/2011 - 1 437U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by tightening the bolt. 437N 15/06/2011 16/06/2011 16/06/2011 - 2 438U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by 1 1 |
| 436U 15/06/2011 16/06/2011 16/06/2011 Moisture and density are not measured. 1 436N 15/06/2011 16/06/2011 16/06/2011 - 1 437U 15/06/2011 16/06/2011 Pre-crack on the side 2 by tightening the bolt. 1 437N 15/06/2011 16/06/2011 16/06/2011 - 2 438U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by 1 |
| 436N 15/06/2011 16/06/2011 16/06/2011 - 1 437U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by tightening the bolt. 437N 15/06/2011 16/06/2011 16/06/2011 - 2 438U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by 1 |
| 436N 15/06/2011 16/06/2011 16/06/2011 - 1 437U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by tightening the bolt. 1 437N 15/06/2011 16/06/2011 16/06/2011 - 2 438U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by 1 |
| 437U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by tightening the bolt. 1 437N 15/06/2011 16/06/2011 16/06/2011 - 2 438U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by 1 |
| tightening the bolt. 437N 15/06/2011 16/06/2011 16/06/2011 - 2 438U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by 1 |
| 437N 15/06/2011 16/06/2011 16/06/2011 - 2 438U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by 1 |
| 438U 15/06/2011 16/06/2011 16/06/2011 Pre-crack on the side 2 by 1 |
| 1000 1 |
| tightening the holt |
| ignoming the bolt. |
| 438N 15/06/2011 16/06/2011 16/06/2011 - 1 |
| 441U 20/06/2011 21/06/2011 21/06/2011 Pre-crack on the side 1 by 1 ⁽¹⁾ |
| tightening the bolt. |
| 441N 20/06/2011 21/06/2011 21/06/2011 - 2 |
| 442U 20/06/2011 21/06/2011 21/06/2011 - 1 ⁽²⁾ |
| 442N 20/06/2011 21/06/2011 21/06/2011 - 2 |
| 443U 20/06/2011 21/06/2011 21/06/2011 Pre-crack on the side 1 by 1 ⁽¹⁾ |
| tightening the bolt. |
| 443N 20/06/2011 21/06/2011 21/06/2011 - 3 444U 20/06/2011 21/06/2011 21/06/2011 Pre-crack on the side 1 by 1 |
| 444U 20/06/2011 21/06/2011 21/06/2011 Pre-crack on the side 1 by 1 ⁽¹⁾ |
| tightening the bolt. |
| 444N 20/06/2011 21/06/2011 21/06/2011 - 2 |
| 445U 21/06/2011 22/06/2011 22/06/2011 Pre-crack on the side 2 by 1 ⁽¹⁾ |
| tightening the bolt. |
| 445N 21/06/2011 22/06/2011 22/06/2011 - 3 |
| 446U 21/06/2011 22/06/2011 22/06/2011 - 1 ⁽³⁾ |
| 446N 21/06/2011 22/06/2011 22/06/2011 - 1 |
| 447U 21/06/2011 22/06/2011 22/06/2011 - 1 ⁽²⁾ |
| 447N 21/06/2011 22/06/2011 22/06/2011 - 3 |
| 448U 21/06/2011 22/06/2011 22/06/2011 - 1 ⁽²⁾ |
| 448N 21/06/2011 22/06/2011 22/06/2011 - 2 |

⁽¹⁾ The type of failure of these tests was failure of the bottom rail. However this type of failure was caused by the presence of the pre-crack, in fact after the bottom rail failure the load increase a lot, sometime more than twice of the failure load, until the type of failure 2, which is the most probable with this test setup. Therefore it can be said that without pre-crack the type of failure would have been the type 2.

⁽²⁾ The type of failure of these tests was failure of the bottom rail. However after the bottom rail failure the load increase a lot, sometime more than twice of the failure load, until the type of failure 2, which is the most probable with this test setup. Probably this was caused by some problem in the rail does not visible. Therefore it can be said that without pre-crack the type of failure would have been the type 2.

⁽³⁾ The test results of this specimen are similar at (2), the only difference is that the second type of failure found were both 2 and 3 together.

Appendix C – Statistical data of test results

| LOAD | | | | | |
|-------------------------|---------------------------|-----------------------------|-------------------------------|-------------------------|-------------------------------|
| Serie 4 - Set 1 Pith UP | Serie 4 - Set 1 Pith DOWN | Serie 4 - Set 1 BIS Pith UP | Serie 4 - Set 1 BIS Pith DOWN | Serie 4 - Set 2 Pith UP | |
| 17745,16 | 22451,50 | 16839,05 | 14986,65 | 17315,35 | |
| 17192,64 | 21010,33 | 18601,15 | 23952,51 | 23036,84 | |
| 10921,86 | 23056,98 | 15560,16 | 17262,99 | 18253,07 | |
| 20589,28 | 23240,51 | 17313,76 | 23682,27 | 20464,28 | |
| 14643,46 | 23675,91 | 19426,37 | 20916,63 | 20767,50 | |
| 21328,24 | 21866,02 | 16808,91 | 23217,45 | 18409,32 | |
| 12971,60 | 20995,53 | 19518,96 | 18293,45 | 15180,25 | |
| 18612,49 | 22531,89 | 15568,87 | 21276,05 | 21018,80 | |
| 16750,59 | 22353,58 | 17454,65 | 20448,50 | 19305,68 | Average [N] |
| 3645,67 | 996,97 | 1577,73 | 3293,50 | 2485,03 | St. Dev. |
| 21,76% | 4,46% | 9,04% | 16,11% | 12,87% | Coeff. Of Var. [%] |
| 8803,03 | 20180,18 | 14015,21 | 13268,68 | 13888,31 | Char. Value 0,05 [|
| DISPLACEMENT 1 | | | | | |
| AT FAILURE | | | | | |
| Serie 4 - Set 1 Pith UP | Serie 4 - Set 1 Pith DOWN | Serie 4 - Set 1 BIS Pith UP | Serie 4 - Set 1 BIS Pith DOWN | Serie 4 - Set 2 Pith UP | |
| 0,012578125 | 0.095585938 | 0,098984375 | -0,007421875 | -0,017265625 | |
| 0,062539063 | -0.01859375 | 0.093320312 | 0,024335938 | 0.07359375 | |
| -0.031992188 | -0.087734375 | 0.010390625 | -0.029570312 | -0.024375 | |
| 0.027734375 | -0.0140625 | -0.010273437 | 0.008046875 | -0.012460937 | |
| 0.021054687 | -0.039414062 | -0,000976563 | 0,00125 | -0,108828125 | |
| 0.034023437 | 0,01875 | 0.024101563 | 0,003789063 | -0.014609375 | |
| -0.013828125 | -0.012109375 | 0,076679687 | 0.047304688 | -0.0003125 | |
| -0.0215625 | -0,198164063 | -0.015273437 | 0,026914062 | 0,019570313 | |
| 0,01 | -0,03 | 0.03 | 0.01 | -0.01 | Average [mm] |
| 0.03 | 0.08 | 0.05 | 0.02 | 0.05 | St. Dev. |
| 281,27% | -265,76% | 137,35% | 251,92% | -479.12% | Coeff. Of Var. [% |
| -0.06 | -0,22 | -0.07 | -0.04 | -0.12 | Char. Value 0.05 [m |
| DISPLACEMENT 2 | | 1000 | 19.306/86/19 | 22,500.0 | The last contract of the same |
| AT FAILURE | | | | | |
| Serie 4 - Set 1 Pith UP | Serie 4 - Set 1 Pith DOWN | Serie 4 - Set 1 BIS Pith UP | Serie 4 - Set 1 BIS Pith DOWN | Serie 4 - Set 2 Pith UP | |
| 0.551132812 | 1.91203125 | 0.571933594 | 0.5509375 | 0.456894531 | |
| 0.628111979 | 1,372929688 | 0.972415365 | 3.077369792 | 1.215019531 | |
| 0,183496094 | 2,331927083 | 0,5634375 | 0,429707031 | 0,403828125 | |
| 0,757897135 | 2,609589844 | 0,436210938 | 2,893997396 | 1,296386719 | |
| 0,326171875 | 1,6121875 | 1,161341146 | 1,342623698 | 1,246236979 | |
| 0,902050781 | 1,661901042 | 0,51061849 | 2,11906901 | 0,342597656 | |
| 0,130410156 | 1,300572917 | 0,754915365 | 0,647871094 | 0,453938802 | |
| 0,804355469 | 2,422447917 | 0,536770833 | 1,441588542 | 0,488606771 | |
| 0,54 | 1,90 | 0,69 | 1,56 | 0,74 | Average [mm] |
| 0,29 | 0.50 | 0.26 | 1,04 | 0,43 | St. Dev. |
| 54,53% | 26.20% | 37,08% | 66.60% | 58,12% | Coeff. Of Var. [% |
| -0.09 | 0.82 | 0.13 | -0.71 | -0.20 | Char. Value 0.05 [m |

| Serie 4 - Set 1 Pith DOWN 50 | Serie 4 - Set 1 BIS Pith UP | | | |
|--|--|--|--|--|
| | Serie 4 - Set I BIS Pith UP | | | |
| 30 | | | | |
| 15/200 | 58 | 53 | 62 | |
| 90 | 57 | 84 | 64 | |
| 60 | 44 | 59 | 53 | |
| (50) | | 0.00 | 77 | |
| | | | | |
| | | - 455 | | |
| 12.5 | | | | |
| 2.7 | 34 | 90 | 58 | |
| 67,25 | 46,75 | 68,00 | 60,00 | Average [mm] |
| 15,29 | 8,15 | 12,56 | 9,35 | St. Dev. |
| 22,73% | 17,44% | 18,47% | 15,58% | Coeff. Of Var. [%] |
| 33,93 | 28,97 | 40,62 | 39,62 | Char. Value 0,05 [mm |
| | | | | |
| Serie 4 - Set 1 Pith DOWN | Serie 4 - Set 1 BIS Pith UP | Serie 4 - Set 1 BIS Pith DOW | N Serie 4 - Set 2 Pith UP | |
| 72 | 67 | 40 | 57 | |
| 52 | 70 | 40 | 55 | |
| 54 | 64 | 44 | 69 | |
| 57 | 70 | 48 | 60 | |
| 60 | 67 | 36 | 104 | |
| 40 | 63 | 40 | 62 | |
| | | | | |
| | | | | |
| 500 PARTY 20 | | THE STATE OF THE S | The second secon | Average [mm] |
| | | | | St. Dev. |
| 1155.507 | 98.50 | 115 W 15 75 75 75 75 75 75 75 75 75 75 75 75 75 | | Coeff. Of Var. [%] |
| 10 A S A S A S A S A S A S A S A S A S A | | | Salar Sa | Char. Value 0,05 [mm |
| 54,50 | 24,02 | | 32.02 | Chart value of the family |
| Serie 4 - Set 1 Pith DOWN | Serie 4 - Set 1 BIS Pith UP | Serie 4 - Set 1 BIS Pith DOW | N Serie 4 - Set 2 Pith UP | |
| 45 | 61 | 54 | 62 | |
| 85 | 60 | 85 | 60 | |
| 55 | 46 | 59 | 60 | |
| 60 | 42 | 59 | 63 | |
| 66 | 1775 | 60 | 81 | |
| | | 457 | 337 | |
| | | | | |
| | 1000 | | 1.00 | |
| NO WISSON | The second secon | 160,000,000 | | Average [mm] |
| Complete in | | | A CONTRACTOR OF THE PARTY OF TH | St. Dev. |
| | | | 5400 | Coeff. Of Var. [%] |
| 10.00000000000000000000000000000000000 | 201 20 NOOD 2010 | | to be supposed to the supposed | Char. Value 0.05 [mm |
| | 22,73% 33,93 Serie 4 - Set 1 Pith DOWN 72 52 54 57 60 40 54 72 57,63 10,61 18,41% 34,50 Serie 4 - Set 1 Pith DOWN 45 85 55 60 | 63 50 50 65 47 54 44 91 34 67,25 46,75 15,29 8,15 22,73% 17,44% 33,93 28,97 Serie 4 - Set 1 Pith DOWN Serie 4 - Set 1 BIS Pith UP 72 67 52 70 54 64 57 70 60 67 40 63 54 62 72 56 57,63 64,88 10,61 4,67 18,41% 7,20% 34,50 54,69 Serie 4 - Set 1 Pith DOWN Serie 4 - Set 1 BIS Pith UP 45 61 85 60 55 46 60 59 51 53 48 91 38 64,25 50,75 15,94 8,83 24,80% 17,39% | 63 50 65 65 67 62 62 62 64 64 91 34 90 66 67.25 46,75 68,00 15.29 8,15 12,56 22,73% 17,44% 18,47% 33,93 28,97 40,62 8erie 4 - Set 1 Pith DOWN Serie 4 - Set 1 BIS Pith UP Serie 4 - Set 1 BIS Pith DOW 52 67 40 40 54 54 64 57 70 48 60 67 36 60 67 36 60 67 57,63 64,88 45,00 10,61 4,67 9,64 18,41% 7,20% 34,50 54,69 23,99 8erie 4 - Set 1 Pith DOWN 545 60 60 67 59 51 60 60 60 59 51 60 60 60 59 51 53 48 60 91 38 66 60 60 59 51 59 60 60 60 59 51 59 60 60 60 59 51 59 60 60 60 59 51 59 60 60 60 59 51 59 60 60 60 59 51 59 60 60 60 59 51 59 60 60 60 59 51 59 60 60 60 59 51 59 60 60 59 51 59 60 60 59 51 59 60 60 59 51 59 60 60 59 51 59 60 60 59 51 59 60 515,94 8,83 12,58 24,80% 17,39% 19,24% | 63 50 65 75 62 44 65 57 62 44 66 57 62 62 64 65 67 691 34 90 58 67,25 46,75 68,00 60,00 15,29 8,15 12,56 9,35 22,73% 17,44% 18,47% 15,58% 33,93 28,97 40,62 39,62 8erie 4 - Set 1 BIS Pith UP 8erie 4 - Set 1 BIS Pith UP 72 67 40 57 70 40 55 54 64 44 69 57 70 48 60 67 36 104 40 62 57 70 48 60 67 36 104 40 62 54 62 55 60 55 67 60 55 66 60 60 81 10,61 4,67 9,64 16,45 18,41% 7,20% 21,41% 24,06% 34,50 54,69 23,99 32,52 8erie 4 - Set 1 Pith DOWN Serie 4 - Set 1 BIS Pith UP 60 60 67 60 68,38 10,61 4,67 9,64 16,45 18,41% 7,20% 21,41% 24,06% 34,50 54,69 23,99 32,52 8erie 4 - Set 1 Pith DOWN Serie 4 - Set 1 BIS Pith UP 8erie 4 - Set 1 BIS Pith DOWN Serie 4 - Set 2 Pith UP 60 60 60 60 81 50 60 60 60 81 50 60 60 60 81 50 60 60 60 81 50 60 60 60 81 50 60 60 60 81 50 60 60 60 81 50 60 60 60 81 50 60 60 60 60 81 50 60 60 60 60 81 50 60 60 60 60 60 60 60 60 60 60 60 60 60 |

| DISTANCE TO CRACK | | | | | |
|-------------------------|--|--|-------------------------------|--|------------------------------|
| FROM ANCHORBOLT 2 | 0 1 4 0 1 1 1 1 1 1 1 1 1 | 0 1 1 0 1 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 | C. I. A. C. I. DIC DIJ DOUG | 0 1 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | |
| Serie 4 - Set 1 Pith UP | | | Serie 4 - Set 1 BIS Pith DOWN | | |
| 60 64 | 83 | 62 | 39 55 | 60 | |
| 65 | 60 | 60 | 44 | 58 | |
| 83 | | 60 | | 68 | |
| 60 | 60 | 60 | 52 36 | 102 | |
| 56 | 44 | 60 | 46 | 58 | |
| 75 | 50 | 60 | 45 | 76 | |
| 78 | 78 | 51 | 63 | 59 | |
| 67.63 | 61.88 | 59.13 | 47.50 | 67.63 | Annual and Ferral A |
| 2007/2007 | TO THE PARTY OF TH | | 49.00000 | CONTRACTOR | Average [mm] |
| 9,78 | 12,99 | 3,36 | 8,80 | 15,25 | St. Dev. |
| 14,47% | 20,99% | 5,68% | 18,52% | 22,55% | Coeff. Of Var. [%] |
| 46,30 | 33,56 | 51,81 | 28,32 | 34,38 | Char. Value 0,05 [mm |
| DENSITY | | | | | |
| Serie 4 - Set 1 Pith UP | | Control of the Contro | Serie 4 - Set 1 BIS Pith DOWN | The state of the s | |
| 442,8614981 | 406,017099 | 364,1825192 | 357,326247 | 390,3217528 | |
| 445,3850348 | 462,3345399 | 396,5118458 | 369,3448624 | 390,4805994 | |
| 421,7424758 | 388,575155 | 382,1961458 | 410,5554113 | 376,8889877 | |
| 434,5583404 | 338,2166578 | 502,8099158 | 432,9280741 | 375,1963088 | |
| 522,790461 | 448,9922807 | 409,7052405 | 393,3269024 | 403,7810073 | |
| 435,0774452 | 442,7566007 | 428,1903654 | 433,0097114 | 436,6177452 | |
| 374,4072421 | 441,7705422 | 424,0516218 | 432,7115989 | 550,4348886 | |
| 411,043541 | 386,5823563 | 391,7814698 | 403,656933 | 471,228207 | |
| 435,98 | 414,41 | 412,43 | 404,11 | 424,37 | Average [kg/m ³] |
| 41,90 | 42,02 | 42,23 | 29,37 | 60,52 | St. Dev. |
| 9,61% | 10,14% | 10,24% | 7,27% | 14,26% | Coeff. Of Var. [%] |
| 344.64 | 322,79 | 320,38 | 340,08 | 292,43 | Char. Value 0,05 [kg/m |
| MOISTURE | | | | | 03/40/ |
| Serie 4 - Set 1 Pith UP | Serie 4 - Set 1 Pith DOWN | Serie 4 - Set 1 BIS Pith UP | Serie 4 - Set 1 BIS Pith DOWN | Serie 4 - Set 2 Pith UP | |
| 12,36525048 | 11,83774834 | 14,05128205 | 13,79613357 | 13,9148073 | |
| 13,8184491 | 14,31860037 | 13,83694839 | 13,83347788 | 10,99691675 | |
| 13.22725012 | 12.44532803 | 13,69574378 | 12,86110012 | 11,88059701 | |
| 14,74916388 | 13,05623472 | 13,02465023 | 13,50519431 | 12,16367713 | |
| 13,75905201 | 12,84982263 | 14,03899721 | 13,585209 | 12,92257361 | |
| 12,79069767 | 13,59969266 | 13,2798574 | 13.62922231 | 13,49960412 | |
| 13,15673289 | 12,3100896 | 13,22525597 | 13,24392288 | 13,28016644 | |
| 12,25266362 | 13,22712116 | 13,51782863 | 12,98701299 | 12,75415896 | |
| 13,26 | 12,96 | 13,58 | 13,43 | 12,68 | Average [%] |
| 0,83 | 0,78 | 0,39 | 0,36 | 0.95 | St. Dev. |
| 6,26% | 6,05% | 2,84% | 2,70% | 7,52% | Coeff. Of Var. [%] |
| 11.45 | 11,25 | 12,74 | 12.64 | 10,60 | Char. Value 0,05 [%] |

| LOAD | | | | | |
|--|--------------------------|---------------------------|--------------------------|---------------------------|--|
| | Serie 4 - Set 3 Pith UP | Serie 4 - Set 3 Pith DOWN | Serie 4 - Set 4 Pith UP | Serie 4 - Set 4 Pith DOWN | |
| 27643.42 | 26575.64 | 31529.84 | 13807.47 | 47372.20 | |
| 29615.78 | 17161.24 | 38469.18 | 24014,67 | 46087.41 | |
| 29506.13 | 34145,47 | 28381.07 | 20249,77 | 41868.31 | |
| 26065.43 | 22564,35 | 37884.18 | 25737.08 | 47952,49 | |
| 26069.02 | 24986,38 | 43987.20 | 19253.06 | 46305.73 | |
| 26333.78 | 23822.10 | 35520.91 | 25930.73 | 45414.18 | |
| 27484,77 | 18467.28 | 44511.85 | 16068.53 | 44277,93 | |
| 31309.78 | 21746.91 | 46611.21 | 15266.15 | 47163,62 | |
| 28003.51 | 23683.67 | 38361,93 | 20040,93 | 45805.23 | Average [N] |
| 1944,73 | 5268,31 | 6460.01 | 4796.21 | 1972.18 | St. Dev. |
| 6.94% | 22,24% | 16.84% | 23,93% | 4,31% | Coeff. Of Var. [%] |
| 23764.00 | 12198.75 | 24279,11 | 9585,20 | 41505.89 | Char. Value 0.05 [N] |
| DISPLACEMENT 1 | 12170,10 | -1-1-1-1-1 | 1200120 | 12230,03 | Chart talac size [:1] |
| AT FAILURE | | | | | |
| | Serie 4 . Set 3 Pith I'P | Serie 4 - Set 3 Pith DOWN | Serie 4 . Set 4 Pith I'P | Serie 4 - Set 4 Pith DOWN | |
| -0.004140625 | 0.03859375 | 0.139101563 | 0.025742187 | 0.16265625 | |
| 0.0228125 | -0.041875 | -0.013320312 | 0.076875 | 0.101484375 | |
| -0.117382812 | 0.062578125 | 0.019257813 | 0.023320313 | 0.071210938 | |
| 0.0265625 | 0.011015625 | 0.01609375 | 0.135898438 | 0.177304687 | |
| -0.018476563 | 0.02859375 | 0.063554687 | 0.007539062 | 0,153554688 | |
| 0.025898437 | 0.049804688 | 0.0353125 | 0.04375 | 0.2609375 | |
| 0.069453125 | -0.00015625 | 0.19734375 | 0.04515625 | 0.118554687 | |
| 0.055078125 | 0.033671875 | 0.095234375 | -0.02953125 | 0.16453125 | |
| 0.01 | 0.02 | 0,07 | 0,04 | 0.15 | Average [mm] |
| 0.06 | 0.03 | 0,07 | 0,05 | 0.06 | St. Dev. |
| 774.15% | 144,29% | 102,79% | 119,77% | 37.87% | Coeff. Of Var. [%] |
| -0.12 | -0.05 | -0.09 | -0.07 | 0.03 | Char. Value 0.05 [mm] |
| DISPLACEMENT 2 | -0,03 | -0,09 | -0,07 | 0,03 | Char. value 0,03 [mm] |
| AT FAILURE | | | | | |
| NAME AND ADDRESS OF THE OWNER, WHEN PARTY OF T | Savia 1 Sat 3 Pith I'D | Serie 4 - Set 3 Pith DOWN | Saria 1 Sat 1 Dith I'D | Serie 4 - Set 4 Pith DOWN | |
| 1.877076823 | 1.293398438 | 2.189915365 | 0.207988281 | 3.060423177 | |
| 1,596184896 | 0.285924479 | 1.960514323 | 1.106640625 | 2.991731771 | |
| 1,644980469 | 2.382441406 | 1.027838542 | 0.424095052 | 2.800891927 | |
| 1,780390625 | 0.796009115 | 2.248183594 | 1.078170573 | 2,994192708 | |
| 1,471601563 | 0.563496094 | 2,374824219 | 0.387766927 | 2,994192708 | |
| 1,367871094 | 0.910625 | 2,061041667 | 1.211783854 | 3,708177083 | |
| 2.027903646 | 0,523463542 | 2,307057292 | 0,305527344 | 3,379270833 | |
| 3.103229167 | 0.565052083 | 2,451510417 | 0.053235677 | 2.973561198 | |
| 1.86 | 0,363032083 | 2,431310417 | 0,033233677 | 3.10 | Average [mm] |
| 0.55 | 0,67 | 0,45 | 0,46 | 0.30 | St. Dev. |
| 29,39% | 72,79% | 21.82% | 76,90% | 9,57% | Coeff. Of Var. [%] |
| 0.67 | -0.54 | 1,09 | -0.40 | 2,45 | THE RESERVE OF THE PARTY OF THE |
| 0,07 | -0,54 | 1,09 | -0,40 | 4,40 | Char. Value 0,05 [mm] |

| DISTANCE TO CRACK | | | | | |
|---------------------------|-------------------------|---------------------------|-------------------------|---------------------------|-----------------------------|
| FROM EDGE SIDE 1 | | | | | |
| | Serie 4 - Set 3 Pith UP | Serie 4 - Set 3 Pith DOWN | Serie 4 - Set 4 Pith UP | Serie 4 - Set 4 Pith DOWN | |
| 68 | 56 | | 57 | | |
| 98 | 55 | 89 | 57 | | |
| 62 | 29 | 54 | 52 | | |
| 82 | 54 | 19 | 47 | | |
| 47 | 57 | 65 | 46 | 75 | |
| 66 | 58 | 80 | 57 | 50 | |
| 59 | 60 | | 63 | | |
| 85 | 54 | 91 | 18 | | |
| 70,88 | 52.88 | 66,33 | 49,63 | 62,50 | Average [mm] |
| 16,39 | 9,86 | 27,22 | 13,98 | 17,68 | St. Dev. |
| 23,13% | 18.65% | 41,03% | 28,17% | 28,28% | Coeff. Of Var. [%] |
| 35.14 | 31,37 | 2,92 | 19.15 | | Char. Value 0,05 [mn |
| DISTANCE TO CRACK | 1717/8711 | | 70.00mm) | | Particle Common State Stoom |
| FROM EDGE SIDE 2 | | | | | |
| Serie 4 - Set 2 Pith DOWN | Serie 4 - Set 3 Pith UP | Serie 4 - Set 3 Pith DOWN | Serie 4 - Set 4 Pith UP | Serie 4 - Set 4 Pith DOWN | |
| 55 | 63 | | 60 | | |
| 54 | 86 | 50 | 59 | | |
| 45 | 59 | 44 | 63 | | |
| 55 | 75 | 14 | 60 | | |
| 55 | 75 | 39 | 68 | 64 | |
| 32 | 80 | 64 | 60 | 24 | |
| 50 | 60 | 1000 | 55 | | |
| 55 | 52 | 69 | 66 | | |
| 50.13 | 68,75 | 46.67 | 61,38 | 44,00 | Average [mm] |
| 8.15 | 11.88 | 19,71 | 4.14 | 28,28 | St. Dev. |
| 16.26% | 17.28% | 42,25% | 6,74% | 64.28% | Coeff. Of Var. [%] |
| 32,36 | 42.86 | 0.73 | 52,35 | - 10-ft 10-10 | Char. Value 0,05 [mn |
| DISTANCE TO CRACK | 1-200000 T | \$40.T | -335,60,60 | | |
| FROM ANCHORBOLT 1 | | | | | |
| Serie 4 - Set 2 Pith DOWN | Serie 4 - Set 3 Pith UP | Serie 4 - Set 3 Pith DOWN | Serie 4 - Set 4 Pith UP | Serie 4 - Set 4 Pith DOWN | |
| 65 | 60 | | 57 | | |
| 88 | 60 | 85 | 57 | | |
| 60 | 30 | 54 | 62 | | |
| 80 | 59 | 18 | 62 | | |
| 52 | 60 | 60 | 41 | 66 | |
| 59 | 59 | 74 | 59 | 54 | |
| 55 | 60 | | 60 | 77 | |
| 82 | 62 | 88 | 30 | | |
| 67.63 | 56.25 | 63,17 | 53,50 | 60,00 | Average [mm] |
| 13.72 | 10.65 | 25,86 | 11,65 | 8,49 | St. Dev. |
| 20,29% | 18.93% | 40,95% | 21,78% | 14,14% | Coeff. Of Var. [%] |
| | | | | | |

| DISTANCE TO CRACK | | | | | |
|---------------------------|--------------------------|---------------------------|--------------------------|---------------------------|------------------------------|
| FROM ANCHORBOLT 2 | | | | | |
| | | Serie 4 - Set 3 Pith DOWN | | Serie 4 - Set 4 Pith DOWN | |
| 62 | 60 | | 59 | | |
| 61 | 81 | 62 | 59 | | |
| 50 | 60 | 48 | 63 | | |
| 60 | 71 | 16 | 60 | | |
| 54 | 72 | 50 | 60 | 60 | |
| 42 | 76 | 72 | 59 | 17 | |
| 42 | 60 | | 59 | | |
| 60 | -57 | 77 | 61 | | |
| 53,88 | 67,13 | 54,17 | 60,00 | 38,50 | Average [mm] |
| 8,36 | 8,98 | 21,97 | 1,41 | 30,41 | St. Dev. |
| 15,51% | 13,38% | 40,56% | 2,36% | 78,98% | Coeff. Of Var. [%] |
| 35,66 | 47,54 | 2,98 | 56,92 | | Char. Value 0,05 [mm] |
| DENSITY | | | | | |
| Serie 4 - Set 2 Pith DOWN | Serie 4 - Set 3 Pith UP | Serie 4 - Set 3 Pith DOWN | Serie 4 - Set 4 Pith UP | Serie 4 - Set 4 Pith DOWN | |
| 393,4410169 | 463,6006074 | 454,9853986 | 370,1469925 | 394,7593494 | |
| 419,4784 | 393,8937568 | 450,3882516 | 468,7823074 | 433,3451878 | |
| 367,5401289 | 488,9644831 | 394,1796118 | 450,7832464 | 384,7178029 | |
| 367,2692428 | 424,71012 | 420,8982532 | 397,9739448 | 410,5799862 | |
| 432,6000389 | 410,8828148 | 449,0444505 | 421,4911751 | 400,4296264 | |
| 409,4173953 | | 378,3341754 | 390,0647246 | 396,3939074 | |
| 389,0288069 | 371,3011501 | 526,0552726 | 384,6931165 | 390,4005585 | |
| 449,8896104 | 432,9828113 | 454,4972488 | 398,5233621 | 379,8159508 | |
| 403,58 | 426,62 | 441.05 | 410,31 | 398,81 | Average [kg/m ³] |
| 29,77 | 40.16 | 45,18 | 34.13 | 16.84 | St. Dev. |
| 7,38% | 9.41% | 10,24% | 8,32% | 4,22% | Coeff. Of Var. [%] |
| 338.68 | 336,66 | 342.56 | 335.91 | 362.08 | Char. Value 0.05 [kg/m |
| MOISTURE | 220,00 | 542,50 | 555,51 | 202,00 | Chair value o,oo [Rg/m |
| Serie 4 - Set 2 Pith DOWN | Serie 4 . Set 3 Pith IIP | Serie 4 - Set 3 Pith DOWN | Serie 4 . Set 4 Pith IIP | Serie 4 - Set 4 Pith DOWN | |
| 13.10427487 | 14.61024499 | 14.4622093 | 10.80139373 | 12.92360712 | |
| 13,45467523 | 11,7671346 | 14.42166911 | 14.20765027 | 12.02961135 | |
| 13,41870824 | 14.02877698 | 12,32876712 | 11,97525409 | 11.65620094 | |
| 12.31988473 | 13.1345689 | 12,89669142 | 11,3317757 | 13.48314607 | |
| 13.9212828 | 13.19444444 | 11,69950739 | 13.13364055 | 12.82240236 | |
| 12,87027579 | 10,1200000 | 13,56740355 | 13.1 | 12.69058296 | |
| 12,02072539 | 13,20868516 | 14,33666191 | 11.20802442 | 10.00446628 | |
| 13,46525097 | 11,52219873 | 11.4589156 | 9,974587039 | 12.30620155 | |
| 13,07 | 13.07 | 13.15 | 11.97 | 12,30020133 | Average [%] |
| 0,64 | 1.11 | 1,23 | 1.41 | 1.07 | St. Dev. |
| 4,89% | 8,51% | 9,37% | 11,81% | 8,70% | Coeff. Of Var. [%] |
| 11.68 | 10.57 | 10.46 | 8.89 | 9,92 | Char. Value 0,05 [%] |

References

- [1] Källsner B., Girhammar U.A. Plastic design of partially anchored wood-framed wall diaphragms with and without openings, Proceedings CIB-W18 Meeting, Karlsruhe, Germany, Paper 38-15-7, 2005.
- [2] Caprolu, G., "Experimental testing of anchoring devices for bottom rails in partially anchored timber frame shear walls", Luleå University of Technology, Department of Civil, Environmental and Natural Resources, Report 2011, Luleå, Sweden 2011.